Evaluating the Dimensionality of the Michigan English Language Assessment Battery

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This study evaluates the dimensionality of Form FF, listening and Form EE, grammar/cloze/vocabulary/reading (GCVR) in the Michigan English Language Assessment Battery (MELAB). It further investigates the influences of gender, native language, and proficiency level on the dimensionality of the listening and the GCVR sections in the MELAB. Stout's procedure was employed to test two hypotheses; that the listening items are unidimensional, and the GCVR items are unidimensional. Principle axes factor analysis and principle component analysis both using the tetrachoric correlation matrix were applied for further exploration. The results indicate that both listening and GCVR tests were unidimensional for female and Tagalog/Filipino-speaking groups. Further, the global GCVR test was unidimensional. But for other groups, the results were inconsistent across methods regarding the unidimensionality of both forms.

Validity is an important issue in test development and evaluation according to the *Standards for Educational and Psychological Testing* (American Educational Research Association, American Psychological Association, & National Council on Measurement in Education, 1999), as well as fairness. Validity refers to the degree to which evidence supports the inferences based on test scores (Messick, 1989). Fairness means that all examinees are given comparable opportunities to demonstrate their abilities on the construct a test intends to measure (American Educational Research Association, et al., 1999, p.74). In examining test fairness, the researcher should address questions such as whether the test measures the same construct in all relevant populations (Wang & Witt, 2002). An investigation of the factor structure of a test can provide evidence of validity (Messick, 1995) and fairness of the test.

To make valid and fair comparisons across examinee groups, test items should be constructed to measure the same construct(s). However, test items often measure other traits in addition to the traits they intend to measure (Hambleton & Swaminathan, 1985; Reckase, 1979, 1985; Stout, 1987). Several studies (Birenbaum & Tatsuoka, 1982; Bock, Gibbons, & Muraki, 1988) indicated that item attributes and examinee characteristics could affect the dimensionality of test items. Dimensionality is a property of the test as well as of the examinees (Reckase, 1990). This is also true with language proficiency tests. Oltman and Stricker (1988) and Kok (1992) showed that examinees' English proficiency and ethnic background affected the dimensionality of language proficiency tests. Therefore, when evaluating the dimensionality of a test, it would provide a better picture if the evaluation were done from the perspective of both the test itself and the examinees' characteristics.

The Michigan English Language Assessment Battery (MELAB) is a test developed for college and university admission. It intends to assess the English language competence of adult non-native speakers of English who will apply to study at an English-speaking institution. The MELAB includes Part 1, writing on a prompt, Part 2, a listening

comprehension test, Part 3, grammar, cloze, vocabulary, and reading comprehension (GCVR) questions, and an optional speaking test. All the items in the listening and GCVR subtests are scored dichotomously.

The *MELAB Technical Manual* (English Language Institute, University of Michigan, 1996) reported factor analysis results, done at the component score level, of Part 2 and Part 3 in the MELAB. The *Michigan English Language Assessment Battery: Technical Manual 2003* (English Language Institute, University of Michigan, 2003) reported an item factor analysis of the individual items in Part 2 and Part 3 sections of the MELAB, and principle component analysis of the testlet scores. The item-level factor analysis provided more information regarding the construct validity of Part 2 and Part 3 in the MELAB.

The purpose of this study is to evaluate the dimensionality of Part 2, listening comprehension, and Part 3, GCVR, in the MELAB separately, using item-level information. It further investigates the influences of gender, native language, and language proficiency level on the dimensionality of the listening comprehension test and the GCVR test. Two sets of hypotheses were proposed for this research. One set was that the items in Part 2 were unidimensional, globally and across subgroups of examinees. The other set was that the items in Part 3 were also unidimensional, globally and across subgroups of examinees. In short, this study intends to provide a better understanding of the dimensionality of Part 2 and Part 3 in the MELAB and to determine the consistency in dimensionality across all available examinees and the selected subgroups of examinees.

Stout's Nonparametric Analysis of Dimensionality

Stout (1987) proposed the concept of essential unidimensionality. Essential unidimensionality refers to the existence of exactly one dominant dimension. Van Abswoude, van der Ark, and Sijtsma (2004) suggest that DIMTEST can be used to verify unidimensionality when there is only one dominant trait in the data set and only a few items are driven by another trait. DIMTEST is a statistical assessment of whether there is one or more than one dominant dimension. Stout's nonparametric procedure (Nandakumar & Stout, 1993; Stout, 1987) tests two statistical hypotheses. The null hypothesis states that d = 1 and the alternative hypothesis is that d > 1, where d stands for the number of dimensions in a set of test items.

To test the hypothesis that a group of dichotomous items is unidimensional, DIMTEST divides all the items on the test into three subtests, two assessment subtests, and one partitioning subtest. DIMTEST selects M items from N items: the total number of items on the test. These M items are called Assessment Subtest 1, or AT1. These items are dimensionally distinct from the rest of the items and measure the same trait. AT1 items can be selected based on expert opinions or based on factor analysis results. DIMTEST can automatically choose the AT1 items through a factor analysis procedure using the tetrachoric correlation matrix. Then, another group of M items are selected from the remaining items so that the difficulty levels of these items are as similar to those of the AT1 items as possible. They are called Assessment Subtest 2, AT2. AT2 has a similar difficulty distribution as does AT1, and is dimensionally similar to the remaining items. AT2 is constructed to reduce the examinee variability bias and the item difficulty bias, which may result in false rejection of the null hypothesis. The remaining items, n = N - 2M, is the Partitioning Subtest, PT. Examinees are divided into subgroups based on their PT scores. Examinees with the same PT

score are assigned into the same PT subgroup. For each PT subgroup, a statistic, t_{LK} , based on the examinees' AT1 subtest scores, and a statistic, t_{BK} , based on the examinees' AT2 subtest scores are calculated (see Nandakumar & Stout, 1993; Stout, 1987, for details). The DIMTEST statistic T is obtained with the following formula:

$$T = \frac{T_L - T_B}{\sqrt{2}}$$

where

$$T_L = \sum_{k=1}^{n-1} t_{Lk}$$
 and $T_B = \sum_{k=1}^{n-1} t_{Bk}$

(k is the number of PT scores, t_{Lk} is the standardized difference between two variance estimates). The first variance estimate is actual observed variance between subgroups k number-correct scores on AT1. The second is the variance between subgroups k number-correct AT1 scores that were predicted under the unidimensional assumption. The first variance estimate will be inflated if the data is multidimensional. The measure of the amount of multidimensionality for subgroup k is t_{Lk} . If unidimensionality holds for subgroup k except for statistical error, the two within-subgroup variance estimates are approximately equal, and $t_{Lk} = 0$. If multidimensionality holds, then $t_{Lk} > 0$. If the test is not long enough, T_L is biased even if unidimensionality holds. Thus, T_B is used to correct the statistical bias in T_L . It is better to apply DIMTEST for tests with the total number of items equal to or larger than 80 items. Van Abswoude, et al. (2004) indicated that DIMTEST has low power for short tests.

Consequently, Stout's statistic, T, is compared with the upper $100(1-\alpha)$ percentile of the standard normal distribution, Z_a , for a desired level of significance, α . When $T < Z_a$, DIMTEST accepts the unidimensionality hypothesis. When $T > Z_a$, DIMTEST rejects the unidimensionality hypothesis. Nandakumar (1991) modified Stout's more conservative statistic and proposed a more powerful statistic with a slightly higher but acceptable type I error rate. This study presents both Stout's conservative statistic T and Nandakumar's more powerful statistic T.

Since DIMTEST uses test scores as a conditioning variable, it shows some positive bias even after correcting for the two types of bias using AT2. To further reduce bias and increase the power of the more powerful statistic T, Stout, Goodwin Froelich, and Gao (2001) proposed a new DIMTEST procedure that uses only one AT subtest.

DIMTEST incorporates a FAC procedure that performs an unrotated principle axis factor analysis of the tetrachoric correlation matrix for the dichotomous data set with maximum interitem correlations estimating communalities. A FAC output file containing the second-factor loadings can be utilized as an input file for the ASN program in automatically selecting AT1 items. When the ASN program uses the second-factor loadings from the output of FAC program to automatically choose AT1 items, the number of AT1 items is also determined automatically to optimize the statistical power (Nandakumar & Stout, 1993). The other output file from the FAC program contains the results of the factor analysis. AT1 items can be selected subjectively based on the FAC output. Three sub-programs in DIMTEST are used in this study: FAC, ASN, and SSC. FAC implements a tetrachoric factor analysis, ASN uses the output from the FAC program to select AT1 and AT2 items, and SSC calculates the DIMTEST statistics.

Principle Component Analysis with Tetrachoric Correlations

Principle component analysis has been used by researchers to assess dimensionality of a set of items (Abedi, 1997). If a large amount of variance can be explained by the first component, the set of items can be considered unidimensional. For dichotomous items, principle components analysis uses tetrachoric correlations to reduce items into a small number of principle components accounting for most of the variance in the items. According to Hatcher (1994), multiple criteria can be used to determine the number of components to retain. They are the eigenvalue, the proportion of variance accounted for, and the interpretability criterion. Kaiser (1960) suggests that a component with an eigenvalue larger than one be retained. Hatcher (1994) suggests retaining any component accounting for at least 10% of the total variance. Reckase (1979) suggests that if the first component explains 20% of the variance of a set of items, the item set is unidimensional. In addition, the interpretation of the retained component should make substantive meaning of the constructs.

Method

Data

The data used in this study were from examinees who took Form EE of the Part 2 (GCVR) and Form FF of the Part 3 (listening) of the MELAB. Their responses to Part 2 and Part 3, and the information on their gender and native language, were collected. There were 1,031 examinees who took Form EE, and 1,650 examinees who took Form FF. Form EE contains 100 items: Items 1 through 30 are grammar items, items 31 through 50 are cloze passage items, items 51 through 80 measure vocabulary, and items 81 through 100 are the reading comprehension items. For Form FF (listening), items 1 through 15 are the short questions, items 16 through 35 are the short conversations, and items 36 through 50 are radio report comprehension items. Table 1 shows the test composition for Form EE and Form FF.

Table 1. Composition for Form EE and Form FF

| Form EE (GCVR) | Item Numbers | Form FF (Listening) | Item Numbers |
|----------------|--------------|---------------------|--------------|
| Grammar | 1 to 30 | Short questions | 1 to 15 |
| Cloze | 31 to 50 | Short conversations | 16 to 35 |
| Vocabulary | 51 to 80 | Radio reports | 36 to 50 |
| Reading | 81 to 100 | | |

In this study, two sets of analyses were carried out. The first set of analyses focuses on the global structure of the test items using all available examinee data, and the second set evaluates the local structure of data across subgroups of test takers that differ with respect to gender, native language, and proficiency level. The selected six sub-groups of examinees were female, male, examinees whose native language was Korean, those whose native language was Tagalog/Filipino, high-proficiency examinees for a particular subtest, and low-proficiency examinees for a particular subtest. For both the listening and GCVR tests, high and low proficiency levels were distinguished by the examinee scale scores. For both subtests, examinees with a scale score of 80 or higher were classified as high proficiency

examinees, and those with a scale score below 80 were categorized as low proficiency examinees. Due to the limited amount of data, only Tagalog/Filipino and Korean language groups were analyzed. Altogether, seven dichotomous response data sets were set up for each subtest; namely, data sets for all available examinees taking a particular subtest, female examinees, male examinees, Tagalog/Filipino speakers, Korean speakers, high-proficiency examinees, and low-proficiency examinees, resulting in 14 data sets. The number of examinees for the seven groups for each subtest is summarized in Table 2.

Table 2. Number of Examinees for Each Data Set

| Listening | Number of Examinees |
|----------------------------|---------------------|
| All examinees | 1,650 |
| Female | 1,257 |
| Male | 393 |
| Tagalog/Filipino | 800 |
| Korean | 141 |
| High listening proficiency | 939 |
| Low listening proficiency | 711 |
| GCVR | |
| All examinees | 1,031 |
| Female | 787 |
| Male | 244 |
| Tagalog/Filipino | 527 |
| Korean | 123 |
| High GCVR proficiency | 528 |
| Low GCVR proficiency | 503 |

Procedure

After the collection of item response data, multiple procedures were adopted to appraise global and local dimensionality of the tests: Stout's DIMTEST procedure, principle axis factoring of tetrachoric correlations, and principle components analysis with LISREL.

To calculate Stout's statistic, test items were split into three subtests: AT1 (assessment subtest 1), AT2 (assessment subtest 2), and PT (partitioning subtest). The items in the AT1 were not specified in advance, but were identified through a principle axis factor analysis of the tetrachoric correlations by the FAC application. The FAC program first ran the tetrachoric factor analysis to calculate the second-factor loadings for the selection of AT1 subtest items set. Only part of the data was used for running FAC, while the rest of the data was used for ASN and SSC runs. The ASN program selected AT1 and AT2 items automatically based on the FAC output, and the SSC program calculated the DIMTEST statistic. SSC assessed the statistical significance of the distinctiveness of the dimensionality between two specified subtests: the Assessment Subtests and the Partitioning Subtest. DIMTSET conservative and more powerful T statistics, and their probabilities, were used as the criteria to evaluate test dimensionality, and $\alpha = 0.05$ was used to determine the significance of the hypothesis test.

Principle axis factoring of tetrachoric correlations was run for each group of examinees. Tetrachoric factor analysis in the DIMTEST was run with the specification of the number of factors. For this study, the number of factors was determined based on the natural groupings of the items. For Form FF, the 50 listening items were divided into three parts, measuring examinee ability to understand short questions, short conversations, and radio reports. For Form EE, the 100 GCVR items were categorized into 4 groups, measuring examinee proficiency in grammar, cloze, vocabulary, and reading comprehension. The resulting number of factors for the tetrachoric factor analysis was determined based on the criteria of the strength of the eigenvalues and the differences between the factor eigenvalues.

To further confirm the results obtained in the principle axis factor analysis and the DIMTEST procedure, LISREL was employed to run a principle component analysis using the tetrachoric correlation matrix. The percentage of variance explained by each factor was employed in determining the number of principle components.

Stout's nonparametric procedure, tetrachoric factor analysis, and principle component analysis using the tetrachoric correlation matrix, were each applied to each of the seven data sets for both test forms. Form EE and Form FF of the MELAB test were analyzed for all available examinees and the six specified subgroups of examinees using DIMTEST, FAC in the DIMTEST, and LISREL. Results based on all the available data and those based on the data from the subgroups were compared to evaluate the global dimensionality and the consistency of local dimensionality across different subgroups of examinees.

Results

Stout's DIMTEST Statistics

Table 3 summarizes the analysis results from Stout's nonparametric procedure to test the unidimensionality of the 14 data sets using DIMTEST. For the listening test, both conservative and the more powerful tests indicated that the test was not unidimensional based on all available examinee responses and for the male subgroup of examinees. However, the listening test was unidimensional at the 0.05 level for the female, Tagalog/Filipino speakers, and both high and low listening proficiency examinee groups. For examinees whose native language was Korean, the listening test was unidimensional based on the conservative statistics, but not unidimensional based on the more powerful statistic.

For the GCVR test, the unidimensionality test was accepted at the 0.05 level for all examinees, females, Tagalog/Filipino speakers, and both high- and low-proficiency subgroups. For the male examinees, the GCVR test was not unidimensional. For the Korean-speaking examinees, the DIMTEST conservative statistic supported unidimensionality, but the more powerful statistic rejected the null hypothesis that the GCVR test was unidimensional.

Table 3. DIMTEST Results

| | DIMTEST Statistics | | | | | |
|----------------------------|--------------------|---------|----------|-----------|--|--|
| | Conservative (T) | | More Pov | verful(T) | | |
| Listening | T | P-value | T | P-value | | |
| All examinees | 1.991 | 0.023 | 2.254 | 0.012 | | |
| Female | 0.805 | 0.210 | 1.034 | 0.151 | | |
| Male | 2.625 | 0.004 | 3.108 | 0.001 | | |
| Tagalog/Filipino | 0.529 | 0.298 | 0.697 | 0.243 | | |
| Korean | 1.457 | 0.073 | 1.943 | 0.026 | | |
| High listening proficiency | 0.282 | 0.389 | 0.404 | 0.343 | | |
| Low listening proficiency | 0.325 | 0.373 | 0.425 | 0.335 | | |
| GCVR | | | | | | |
| All examinees | -0.500 | 0.692 | -0.473 | 0.682 | | |
| Female | 1.088 | 0.138 | 1.421 | 0.078 | | |
| Male | 1.802 | 0.036 | 2.148 | 0.016 | | |
| Tagalog/Filipino | -3.441 | 0.9997 | -4.159 | 0.99998 | | |
| Korean | 1.288 | 0.099 | 2.176 | 0.015 | | |
| High GCVR proficiency | -0.413 | 0.66 | -0.485 | 0.686 | | |
| Low GCVR proficiency | 0.071 | 0.472 | -0.004 | 0.502 | | |

Eigenvalues and Eigenvalue Differences

The eigenvalues and the eigenvalue differences between factors for the listening test are summarized in Table 4. The eigenvalues for the first three factors were all larger than 1 for all groups. For all examinees, female, male, Tagalog/Filipino, and Korean-speaking examinee groups, the eigenvalues for the first factor were larger than 10, and the difference between the first two factors was around 10. Hattie (1985) suggests using the difference between the first factor and the second factor divided by the difference between the second and the third factor to examine the relative strength of the first factor (dubbed the Factor Difference Ratio Index (FDRI) in Johnson, Yamashiro, & Yu, 2003). If this ratio is larger than 3, the first factor is relatively strong. Based on this criterion, the data for six examinee groups: all examinees, female, male, Tagalog/Filipino speakers, Korean speakers, and low listening proficiency, satisfy this criterion. The first factor was relatively strong for these six groups of examinees. For the examinee group with high listening proficiency, the eigenvalues for the three factors were of similar strength, around 5. This data set did not meet the FDRI criterion suggested by Hattie (1985).

The eigenvalues and the eigenvalue differences between factors for the GCVR data are summarized in Table 5. The eigenvalues for the first four factors were larger than 1 for all groups. The eigenvalues for the first factor was larger than 10 for all groups, but the FDRI was greater than 3 for only all examinees, female, male, Tagalog/Filipino, and low-GCVR-proficiency examinee groups. The examinee group with high GCVR proficiency and the Korean subgroup did not satisfy Hattie's (1985) FDRI recommendation.

Table 4. Eigenvalues from Tetrachoric Factor Analysis — Listening

| Listening | Factor | Eigenvalue | Difference | FDRI |
|----------------------------|--------|------------|------------|-------|
| All examinees | 1 | 12.133 | 10.477 | 22.68 |
| | 2 | 1.655 | 0.462 | |
| | 3 | 1.193 | 0.182 | |
| Female | 1 | 11.994 | 10.297 | 23.83 |
| | 2 | 1.698 | 0.431 | |
| | 3 | 1.266 | 0.153 | |
| Male | 1 | 12.810 | 9.917 | 11.17 |
| | 2 | 2.893 | 0.888 | |
| | 3 | 2.005 | 0.306 | |
| Tagalog/Filipino | 1 | 11.914 | 10.086 | 20.80 |
| | 2 | 1.828 | 0.485 | |
| | 3 | 1.343 | 0.218 | |
| Korean | 1 | 13.903 | 10.217 | 17.32 |
| | 2 | 3.685 | 0.590 | |
| | 3 | 3.095 | 0.414 | |
| High listening proficiency | 1 | 5.993 | 1.153 | 1.63 |
| | 2 | 4.839 | 0.708 | |
| | 3 | 4.132 | 0.674 | |
| Low listening proficiency | 1 | 5.602 | 3.996 | 26.29 |
| | 2 | 1.606 | 0.152 | |
| | 3 | 1.454 | 0.246 | |

FDRI = factor difference ratio index ((F1-F2)/(F2-F3)).

Table 5. Eigenvalues from Tetrachoric Factor Analysis — GCVR

| GCVR | Factor | Eigenvalue | Difference | FDRI |
|------------------|--------|------------|------------|-------|
| All examinees | 1 | 26.423 | 20.510 | 5.79 |
| | 2 | 5.912 | 3.542 | |
| | 3 | 2.370 | 0.291 | |
| | 4 | 2.079 | 0.576 | |
| Female | 1 | 25.147 | 18.838 | 5.21 |
| | 2 | 6.308 | 3.616 | |
| | 3 | 2.692 | 0.467 | |
| | 4 | 2.225 | 0.430 | |
| Male | 1 | 30.771 | 25.005 | 11.03 |
| | 2 | 5.767 | 2.267 | |
| | 3 | 3.500 | 0.807 | |
| | 4 | 2.693 | 0.171 | |
| Tagalog/Filipino | 1 | 22.959 | 16.987 | 16.92 |
| | 2 | 5.972 | 1.004 | |
| | 3 | 4.968 | 0.342 | |
| _ | 4 | 4.626 | 0.681 | |

Table 5. (cont.)

| GCVR | Factor | Eigenvalue | Difference | FDRI |
|-----------------------|--------|------------|------------|------|
| Korean | 1 | 16.148 | 6.426 | 1.40 |
| | 2 | 9.722 | 4.603 | |
| | 3 | 5.119 | 0.776 | |
| | 4 | 4.343 | 0.351 | |
| High GCVR proficiency | 1 | 11.886 | 3.427 | 2.69 |
| | 2 | 8.460 | 1.272 | |
| | 3 | 7.187 | 2.118 | |
| | 4 | 5.069 | 0.696 | |
| Low GCVR proficiency | 1 | 11.729 | 7.176 | 4.17 |
| | 2 | 4.553 | 1.719 | |
| | 3 | 2.834 | 0.180 | |
| | 4 | 2.654 | 0.726 | |

FDRI = factor difference ratio index ((F1-F2)/(F2-F3)).

Percentage of Variance Explained

To further check the results from the tetrachoric factor analysis in DIMTEST, principle component analysis using the tetrachoric correlation matrix was run in LISREL. The analysis results from LISREL are summarized in Table 6 for the listening test and Table 7 for the GCVR test. For the eigenvalue, a similar pattern to that based on DIMTEST tetrachoric factor analysis results was observed for both listening and GCVR tests using LISREL. Using Reckase's (1979) suggestion that a set of test items is unidimensional if the first factor accounts for 20% or more of the total variance, for the listening test, the item responses of all examinees, females, males, Tagalog/Filipino speakers, and Korean speakers are unidimensional. However, the first principle component for the high and low listening proficiency groups accounted for much less than 20% of the total variance.

For the GCVR test, the first factor for the examinee groups of all examinees, female, male, and Tagalog/Filipino speakers accounted for more than 20% of the total variance. For the Korean speakers and high- and low-GCVR-proficiency examinee groups, the first principle component accounted for less than 20% of the total variance.

The results regarding the dimensionality of the data sets for the listening and the GCVR tests in the MELAB are summarized in Table 8. In most cases, different procedures and evaluation criteria led to different conclusions regarding the dimensionality of the test data. Only data sets from 5 out of 14 groups of examinees yielded consistent conclusions. The listening test for female and Tagalog/Filipino-speaking groups, and the GCVR test for female, Tagalog/Filipino speakers, and all examinees were unidimensional consistently across all procedures used in this study.

Summary and Discussion

Regarding the global dimensionality of Form EE (GCVR test) in the MELAB, unidimensionality held. This is consistent with the item-level factor analysis results reported in the MELAB technical manual 2003 for Part 3. On the other hand, inconsistent results were obtained regarding the global unidimensionality of Form FF (listening test).

Table 6. Eigenvalues from LISREL – Listening

| Listening | | PC 1 | PC 2 | PC 3 |
|----------------------------|------------|-------|-------|-------|
| All examinees | Eigenvalue | 12.69 | 2.26 | 1.80 |
| | % Variance | 25.38 | 4.52 | 3.60 |
| | Cum. % Var | 25.38 | 29.89 | 33.49 |
| Female | Eigenvalue | 12.55 | 2.30 | 1.87 |
| | % Variance | 25.10 | 4.59 | 3.73 |
| | Cum. % Var | 25.10 | 29.69 | 33.42 |
| Male | Eigenvalue | 13.24 | 3.03 | 2.24 |
| | % Variance | 26.47 | 6.07 | 4.48 |
| | Cum. % Var | 26.47 | 32.54 | 37.02 |
| Tagalog/Filipino | Eigenvalue | 12.45 | 2.39 | 1.94 |
| | % Variance | 24.90 | 4.79 | 3.88 |
| | Cum. % Var | 24.90 | 29.69 | 33.57 |
| Korean | Eigenvalue | 14.15 | 3.79 | 3.15 |
| | % Variance | 28.30 | 7.58 | 6.31 |
| | Cum. % Var | 28.30 | 35.89 | 42.19 |
| High listening proficiency | Eigenvalue | 4.81 | 4.14 | 3.46 |
| | % Variance | 9.62 | 8.28 | 6.39 |
| | Cum. % Var | 9.62 | 17.91 | 24.83 |
| Low listening proficiency | Eigenvalue | 6.18 | 2.33 | 2.18 |
| | % Variance | 12.36 | 4.65 | 4.37 |
| | Cum. % Var | 12.36 | 17.01 | 21.38 |

Table 7. Eigenvalues from LISREL — GCVR

| GCVR | | PC 1 | PC 2 | PC 3 | PC 4 |
|------------------|------------|-------|-------|-------|-------|
| All examinees | Eigenvalue | 26.90 | 6.41 | 2.84 | 2.56 |
| | % Variance | 26.90 | 6.41 | 2.84 | 2.56 |
| | Cum. % Var | 26.90 | 33.32 | 36.15 | 38.72 |
| Female | Eigenvalue | 25.61 | 6.81 | 3.17 | 2.78 |
| | % Variance | 25.61 | 6.81 | 3.17 | 2.78 |
| | Cum. % Var | 25.61 | 32.42 | 35.59 | 38.37 |
| Male | Eigenvalue | 31.08 | 6.13 | 3.60 | 3.09 |
| | % Variance | 31.08 | 6.13 | 3.60 | 3.09 |
| | Cum. % Var | 31.08 | 37.21 | 40.81 | 43.90 |
| Tagalog/Filipino | Eigenvalue | 22.03 | 7.57 | 6.39 | 4.35 |
| | % Variance | 22.03 | 7.57 | 6.39 | 4.35 |
| | Cum. % Var | 22.03 | 29.60 | 35.99 | 40.34 |

Table 7. (cont.)

| GCVR | | PC 1 | PC 2 | PC 3 | PC 4 |
|-----------------------|------------|-------|-------|-------|-------|
| Korean | Eigenvalue | 16.49 | 10.07 | 5.48 | 4.76 |
| | % Variance | 16.49 | 10.07 | 5.48 | 4.76 |
| | Cum. % Var | 16.49 | 26.56 | 32.05 | 36.80 |
| High GCVR proficiency | Eigenvalue | 12.35 | 8.86 | 6.32 | 4.73 |
| | % Variance | 12.35 | 8.86 | 6.32 | 4.73 |
| | Cum. % Var | 12.35 | 21.21 | 27.53 | 32.27 |
| Low GCVR proficiency | Eigenvalue | 12.26 | 5.18 | 3.50 | 3.30 |
| | % Variance | 12.26 | 5.18 | 3.50 | 3.30 |
| | Cum. % Var | 12.26 | 17.43 | 20.93 | 24.23 |

Table 8. Results Summary

| | DIMTEST | statistics | | |
|----------------------------|--------------|---------------|-----------------------|--|
| Listening | Conservative | More powerful | Eigenvalue difference | Percentage of variance explained by first factor |
| All examinees | N | N | U | U |
| Female | U | U | U | U |
| Male | N | N | U | U |
| Tagalog/Filipino | U | U | U | U |
| Korean | U | N | U | U |
| High listening proficiency | U | U | N | N |
| Low listening proficiency | U | U | U | N |
| GCVR | | | | |
| All examinees | U | U | U | U |
| Female | U | U | U | U |
| Male | N | N | U | U |
| Tagalog/Filipino | U | U | U | U |
| Korean | U | N | N | N |
| High GCVR proficiency | U | U | N | N |
| Low GCVR proficiency | U | U | U | N |

For each of the studied subgroups of examinees, unidimensionality held for both forms for female and Tagalog/Filipino-speaking examinee groups. For other subgroups of examinees, the results regarding the unidimensionality for each of the two forms were inconsistent in terms of the evaluation criteria adopted in this study. Thus, no conclusion can be drawn regarding the dimensionality of the listening and GCVR sections of the test for those groups of examinees. The dimensionality was not consistent across different groups of examinees for each test form.

Several issues need attention regarding the generalizability of the study results. The first issue is related to the sample size in this study. Hatcher (1994) suggested that the minimal sample size should be 5 times the number of variables to be analyzed. Van Abswoude, et al. (2004) suggested that DIMTEST may be more effective for large sample sizes, such as n = 2,000. However, there were only data for 1,031 examinees available for the GCVR test, and 1,650 examinees for the listening test. When the subgroups of examinees were selected from these samples, much smaller samples resulted. For example, for the male and Korean groups, there were fewer than 400 cases. Sample sizes smaller than that desired may affect the analysis results.

Stout's nonparametric procedure requires selection of the AT1 items, which was completed automatically by the program based on the second-factor loadings and other output from the FAC analysis. This study also tried to manually select AT1 items based on the tetrachoric factor analysis results. However, such selection may lead to the failure of the Wilcoxon Rank Sum Test in the ASN program. Thus, expert opinions and the factor loadings from the tetrachoric factor analysis presented in Table A.1 to Table B.7 in Appendices A and B may be combined to come up with a set of AT1 items. This may improve the DIMTEST procedure for assessing dimensionality.

In summary, the results of this study provide more information regarding the dimensionality of Part 2, listening, and Part 3, GCVR, in the MELAB. This study helps to identify the effect of the test items and of the examinees' characteristics on the dimensionality of the MELAB sections.

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Appendix A

Factor Loadings for Form FF-Listening

Table A.1. Factor Loadings for Listening-All Examinees

| Item | | Factor Loadings | | | |
|------|-------|-----------------|--------|--|--|
| | 1 | 2 | 3 | | |
| 1 | 0.611 | -0.078 | -0.162 | | |
| 2 | 0.376 | 0.056 | -0.199 | | |
| 3 | 0.687 | -0.137 | -0.122 | | |
| 4 | 0.433 | 0.076 | 0.086 | | |
| 5 | 0.435 | 0.024 | -0.221 | | |
| 6 | 0.582 | -0.161 | -0.218 | | |
| 7 | 0.645 | -0.088 | -0.186 | | |
| 8 | 0.544 | 0.041 | -0.101 | | |
| 9 | 0.547 | 0.097 | -0.284 | | |
| 10 | 0.330 | -0.051 | -0.056 | | |
| 11 | 0.244 | -0.015 | -0.149 | | |
| 12 | 0.566 | -0.153 | 0.063 | | |
| 13 | 0.386 | 0.104 | -0.146 | | |
| 14 | 0.407 | 0.133 | -0.080 | | |
| 15 | 0.555 | 0.124 | -0.111 | | |
| 16 | 0.579 | -0.348 | 0.041 | | |
| 17 | 0.686 | -0.054 | -0.044 | | |
| 18 | 0.484 | -0.096 | 0.093 | | |
| 19 | 0.572 | -0.153 | 0.187 | | |
| 20 | 0.655 | -0.002 | 0.014 | | |
| 21 | 0.413 | -0.052 | -0.108 | | |
| 22 | 0.665 | -0.239 | 0.090 | | |
| 23 | 0.737 | -0.147 | -0.058 | | |
| 24 | 0.530 | -0.084 | 0.141 | | |
| 25 | 0.326 | -0.153 | 0.219 | | |
| 26 | 0.576 | -0.110 | -0.024 | | |
| 27 | 0.424 | 0.066 | -0.243 | | |
| 28 | 0.701 | -0.192 | 0.179 | | |
| 29 | 0.696 | -0.226 | -0.015 | | |
| 30 | 0.368 | -0.005 | -0.226 | | |
| 31 | 0.481 | 0.070 | -0.022 | | |
| 32 | 0.513 | -0.216 | 0.134 | | |
| 33 | 0.485 | 0.184 | -0.091 | | |
| 34 | 0.512 | 0.305 | -0.113 | | |
| 35 | 0.312 | 0.048 | 0.063 | | |
| 36 | 0.515 | -0.037 | 0.273 | | |
| 37 | 0.383 | 0.279 | 0.081 | | |
| 38 | 0.314 | 0.159 | 0.011 | | |
| 39 | 0.098 | 0.110 | 0.140 | | |
| 40 | 0.505 | 0.054 | 0.005 | | |

| 41 | 0.360 | 0.240 | 0.176 |
|----|-------|-------|--------|
| 42 | 0.339 | 0.280 | 0.145 |
| 43 | 0.449 | 0.007 | 0.372 |
| 44 | 0.515 | 0.163 | 0.215 |
| 45 | 0.495 | 0.158 | 0.322 |
| 46 | 0.259 | 0.502 | 0.012 |
| 47 | 0.418 | 0.243 | 0.128 |
| 48 | 0.270 | 0.166 | 0.118 |
| 49 | 0.260 | 0.518 | -0.072 |
| 50 | 0.332 | 0.198 | 0.068 |

Table A.2. Factor Loadings for Listening-Female

| Item | | Factor Loading | gs |
|------|-------|----------------|--------|
| | 1 | 2 | 3 |
| 1 | 0.620 | -0.079 | -0.158 |
| 2 | 0.393 | 0.006 | -0.202 |
| 3 | 0.658 | -0.176 | -0.076 |
| 4 | 0.441 | 0.056 | 0.059 |
| 5 | 0.431 | -0.009 | -0.139 |
| 6 | 0.574 | -0.200 | -0.221 |
| 7 | 0.668 | -0.053 | -0.165 |
| 8 | 0.528 | 0.011 | -0.133 |
| 9 | 0.517 | 0.049 | -0.308 |
| 10 | 0.350 | 0.020 | -0.036 |
| 11 | 0.210 | -0.121 | -0.168 |
| 12 | 0.564 | -0.126 | -0.011 |
| 13 | 0.390 | 0.155 | -0.175 |
| 14 | 0.399 | 0.075 | -0.100 |
| 15 | 0.547 | 0.074 | -0.143 |
| 16 | 0.580 | -0.365 | 0.122 |
| 17 | 0.678 | -0.124 | -0.019 |
| 18 | 0.497 | -0.087 | 0.104 |
| 19 | 0.565 | -0.132 | 0.153 |
| 20 | 0.611 | -0.009 | 0.103 |
| 21 | 0.427 | -0.004 | -0.197 |
| 22 | 0.642 | -0.190 | 0.043 |
| 23 | 0.726 | -0.128 | -0.064 |
| 24 | 0.531 | -0.007 | 0.128 |
| 25 | 0.352 | -0.109 | 0.202 |
| 26 | 0.605 | -0.143 | 0.035 |
| 27 | 0.388 | 0.067 | -0.248 |

40

0.535

0.054

| 28 | 0.704 | -0.196 | 0.200 |
|----|-------|--------|--------|
| 29 | 0.706 | -0.254 | 0.005 |
| 30 | 0.375 | -0.038 | -0.200 |
| 31 | 0.477 | 0.004 | 0.017 |
| 32 | 0.510 | -0.119 | 0.095 |
| 33 | 0.499 | 0.204 | -0.147 |
| 34 | 0.507 | 0.344 | -0.187 |
| 35 | 0.320 | 0.015 | 0.068 |
| 36 | 0.502 | -0.046 | 0.344 |
| 37 | 0.373 | 0.286 | 0.091 |
| 38 | 0.324 | 0.179 | 0.052 |
| 39 | 0.112 | 0.098 | 0.080 |
| 40 | 0.515 | 0.107 | -0.111 |
| 41 | 0.367 | 0.214 | 0.206 |
| 42 | 0.340 | 0.300 | 0.189 |
| 43 | 0.460 | 0.056 | 0.341 |
| 44 | 0.531 | 0.162 | 0.179 |
| 45 | 0.474 | 0.187 | 0.323 |
| 46 | 0.221 | 0.515 | -0.023 |
| 47 | 0.410 | 0.318 | 0.104 |
| 48 | 0.279 | 0.191 | 0.087 |
| 49 | 0.245 | 0.478 | -0.127 |
| 50 | 0.345 | 0.187 | 0.052 |

Table A.3. Factor Loadings for Listening-Male

| Item | I | Factor Loading | gs |
|------|-------|----------------|--------|
| | 1 | 2 | 3 |
| 1 | 0.585 | 0.005 | -0.007 |
| 2 | 0.312 | 0.113 | 0.268 |
| 3 | 0.780 | -0.013 | 0.004 |
| 4 | 0.402 | 0.072 | 0.035 |
| 5 | 0.442 | 0.148 | 0.023 |
| 6 | 0.625 | 0.084 | -0.023 |
| 7 | 0.565 | -0.047 | -0.030 |
| 8 | 0.593 | 0.139 | -0.121 |
| 9 | 0.641 | 0.149 | 0.145 |
| 10 | 0.267 | -0.056 | -0.201 |
| 11 | 0.308 | 0.862 | -0.308 |
| 12 | 0.570 | -0.162 | -0.219 |
| 13 | 0.380 | -0.128 | 0.084 |
| 14 | 0.440 | 0.018 | 0.197 |
| 15 | 0.581 | 0.097 | 0.199 |
| 16 | 0.585 | -0.958 | 0.414 |
| 17 | 0.706 | 0.017 | 0.097 |
| 18 | 0.431 | -0.175 | -0.057 |
| 19 | 0.590 | -0.056 | -0.200 |

| 20 | 0.783 | 0.099 | 0.009 |
|----|-------|--------|--------|
| 21 | 0.384 | -0.286 | -0.068 |
| 22 | 0.731 | -0.229 | -0.393 |
| 23 | 0.773 | -0.082 | -0.353 |
| 24 | 0.538 | -0.378 | -0.170 |
| 25 | 0.232 | -0.130 | -0.181 |
| 26 | 0.479 | 0.033 | 0.069 |
| 27 | 0.532 | -0.011 | 0.057 |
| 28 | 0.692 | -0.034 | -0.112 |
| 29 | 0.645 | 0.117 | -0.253 |
| 30 | 0.339 | 0.215 | 0.041 |
| 31 | 0.503 | 0.193 | 0.264 |
| 32 | 0.533 | -0.279 | -0.291 |
| 33 | 0.442 | 0.024 | 0.213 |
| 34 | 0.589 | -0.316 | 0.505 |
| 35 | 0.288 | 0.115 | 0.106 |
| 36 | 0.569 | 0.049 | 0.073 |
| 37 | 0.418 | 0.238 | 0.040 |
| 38 | 0.287 | 0.019 | 0.110 |
| 39 | 0.049 | -0.077 | 0.008 |
| 40 | 0.610 | 0.002 | -0.178 |
| 41 | 0.340 | 0.209 | 0.225 |
| 42 | 0.345 | 0.149 | 0.184 |
| 43 | 0.405 | -0.024 | -0.198 |
| 44 | 0.462 | 0.099 | -0.078 |
| 45 | 0.553 | 0.151 | -0.170 |
| 46 | 0.391 | 0.218 | 0.343 |
| 47 | 0.452 | 0.071 | 0.036 |
| 48 | 0.247 | 0.130 | 0.130 |
| 49 | 0.312 | 0.416 | 0.367 |
| | | | |

Table A.4. Factor Loadings for Listening-Tagalog/Filipino

0.207

0.151

0.289

50

| Item | | Factor Loading | gs |
|------|-------|----------------|--------|
| | 1 | 2 | 3 |
| 1 | 0.598 | -0.106 | -0.138 |
| 2 | 0.399 | -0.001 | -0.147 |
| 3 | 0.686 | -0.211 | -0.053 |
| 4 | 0.452 | 0.148 | 0.147 |
| 5 | 0.448 | -0.072 | -0.267 |
| 6 | 0.556 | -0.120 | -0.146 |
| 7 | 0.663 | -0.048 | -0.220 |
| 8 | 0.532 | 0.061 | -0.064 |
| 9 | 0.581 | 0.177 | -0.261 |
| 10 | 0.321 | -0.026 | -0.043 |
| 11 | 0.216 | 0.023 | -0.143 |
| | | | |

| 12 | 0.515 | -0.121 | 0.122 | 4 | 0.473 | -0.147 | -0.198 |
|---------|------------|----------|----------------|----|-------|--------|--------|
| 13 | 0.376 | 0.181 | -0.101 | 5 | 0.501 | 0.130 | 0.163 |
| 14 | 0.418 | 0.150 | 0.035 | 6 | 0.574 | 0.027 | -0.159 |
| 15 | 0.541 | 0.114 | -0.139 | 7 | 0.715 | -0.025 | -0.015 |
| 16 | 0.520 | -0.392 | -0.020 | 8 | 0.535 | -0.013 | -0.074 |
| 17 | 0.712 | -0.034 | -0.019 | 9 | 0.603 | 0.228 | 0.030 |
| 18 | 0.500 | -0.115 | 0.083 | 10 | 0.374 | 0.176 | 0.017 |
| 19 | 0.526 | -0.294 | 0.122 | 11 | 0.455 | 0.430 | 0.435 |
| 20 | 0.592 | 0.030 | -0.083 | 12 | 0.712 | -0.162 | -0.080 |
| 21 | 0.421 | 0.127 | -0.111 | 13 | 0.664 | 0.105 | -0.206 |
| 22 | 0.668 | -0.152 | 0.147 | 14 | 0.351 | 0.176 | 0.096 |
| 23 | 0.711 | -0.160 | -0.078 | 15 | 0.607 | 0.096 | 0.139 |
| 24 | 0.512 | 0.004 | 0.052 | 16 | 0.866 | -0.167 | -0.786 |
| 25 | 0.334 | -0.291 | 0.266 | 17 | 0.722 | -0.171 | -0.110 |
| 26 | 0.581 | -0.133 | -0.120 | 18 | 0.747 | -0.387 | 0.334 |
| 27 | 0.440 | 0.188 | -0.273 | 19 | 0.675 | -0.415 | 0.381 |
| 28 | 0.659 | -0.301 | 0.078 | 20 | 0.719 | -0.001 | -0.042 |
| 29 | 0.693 | -0.336 | -0.049 | 21 | 0.459 | -0.116 | -0.212 |
| 30 | 0.345 | -0.011 | -0.268 | 22 | 0.480 | -0.228 | 0.012 |
| 31 | 0.505 | 0.093 | 0.087 | 23 | 0.708 | -0.062 | 0.031 |
| 32 | 0.539 | -0.135 | 0.104 | 24 | 0.441 | 0.055 | -0.216 |
| 33 | 0.459 | 0.153 | -0.163 | 25 | 0.384 | -0.176 | 0.501 |
| 34 | 0.514 | 0.385 | -0.170 | 26 | 0.566 | -0.110 | -0.064 |
| 35 | 0.316 | 0.080 | 0.139 | 27 | 0.001 | 0.660 | 0.534 |
| 36 | 0.510 | 0.004 | 0.215 | 28 | 0.793 | -0.493 | 0.420 |
| 37 | 0.424 | 0.266 | 0.092 | 29 | 0.666 | -0.027 | 0.140 |
| 38 | 0.353 | 0.078 | -0.036 | 30 | 0.322 | 0.128 | 0.191 |
| 39 | 0.097 | 0.146 | 0.237 | 31 | 0.214 | 0.025 | -0.170 |
| 40 | 0.490 | 0.085 | -0.047 | 32 | 0.535 | 0.154 | -0.037 |
| 41 | 0.351 | 0.178 | 0.076 | 33 | 0.468 | 0.362 | 0.157 |
| 42 | 0.375 | 0.112 | 0.158 | 34 | 0.461 | 0.238 | -0.063 |
| 43 | 0.444 | 0.120 | 0.389 | 35 | 0.431 | 0.010 | 0.192 |
| 44 | 0.530 | 0.114 | 0.203 | 36 | 0.554 | -0.086 | -0.097 |
| 45 | 0.456 | 0.004 | 0.337 | 37 | 0.412 | -0.048 | 0.010 |
| 46 | 0.211 | 0.431 | 0.125 | 38 | 0.481 | 0.121 | -0.470 |
| 47 | 0.455 | 0.312 | 0.096 | 39 | 0.145 | -0.097 | -0.128 |
| 48 | 0.263 | 0.006 | 0.286 | 40 | 0.353 | 0.298 | -0.324 |
| 49 | 0.249 | 0.491 | -0.025 | 41 | 0.333 | 0.429 | 0.339 |
| 50 | 0.376 | 0.207 | 0.182 | 42 | 0.288 | 0.345 | 0.034 |
| | | | | 43 | 0.530 | -0.183 | -0.145 |
| Table A | .5. Factor | Loadings | for Listening- | 44 | 0.507 | 0.091 | 0.126 |
| Korean | | - | - | 45 | 0.545 | 0.188 | -0.015 |
| | | | | | | | |

Ta K

| Corean | | | |
|--------|-------|---------------|--------|
| Item | F | actor Loading | ıs |
| | 1 | 2 | 3 |
| _ | 1 | 2 | 3 |
| | 0.639 | -0.044 | -0.287 |
| 2 | 0.370 | 0.242 | 0.105 |
| | | - | |
| 3 | 0.763 | 0.101 | 0.041 |

Table A.6. Factor Loadings for Listening-High Proficiency

| Item | F | actor Loading | js |
|------|--------|---------------|--------|
| | 1 | 2 | 3 |
| 1 | 0.450 | 0.054 | 0.119 |
| 2 | 0.137 | 0.510 | 0.170 |
| 3 | 0.462 | 0.074 | 0.285 |
| 4 | 0.345 | -0.144 | -0.315 |
| 5 | 0.314 | -0.057 | 0.407 |
| 6 | 0.477 | -0.169 | -0.004 |
| 7 | 0.145 | 0.018 | 0.139 |
| 8 | 0.128 | 0.175 | 0.067 |
| 9 | 0.022 | 0.169 | -0.051 |
| 10 | 0.076 | 0.060 | 0.025 |
| 11 | -0.026 | 0.586 | -0.387 |
| 12 | 0.524 | -0.489 | -0.373 |
| 13 | 0.199 | 0.080 | 0.096 |
| 14 | 0.420 | 0.072 | 0.053 |
| 15 | 0.506 | 0.231 | 0.010 |
| 16 | -1.498 | 0.316 | -0.420 |
| 17 | -0.024 | 0.056 | -0.270 |
| 18 | 0.306 | 0.368 | 0.314 |
| 19 | -0.133 | -1.405 | -0.043 |
| 20 | -0.474 | 0.620 | 0.317 |
| 21 | 0.152 | 0.152 | 0.008 |
| 22 | -0.346 | -0.026 | 0.138 |
| 23 | 0.695 | 0.302 | -0.493 |
| 24 | -0.035 | 0.161 | -0.095 |
| 25 | 0.282 | -0.135 | 0.045 |
| 26 | 0.317 | 0.206 | 0.331 |
| 27 | 0.381 | 0.370 | 0.085 |
| 28 | -0.179 | 0.059 | 1.388 |
| 29 | 0.463 | 0.380 | -0.238 |
| 30 | 0.026 | 0.193 | 0.017 |
| 31 | -0.034 | 0.459 | 0.066 |
| 32 | 0.335 | -0.134 | 0.078 |
| 33 | 0.082 | 0.135 | -0.018 |
| 34 | 0.133 | 0.188 | 0.188 |
| 35 | 0.128 | -0.097 | -0.009 |
| 36 | -0.110 | 0.422 | -0.451 |
| 37 | -0.086 | 0.102 | -0.008 |
| 38 | 0.022 | 0.061 | -0.098 |
| 39 | 0.013 | 0.007 | -0.028 |
| 40 | -0.006 | 0.233 | 0.146 |
| 41 | -0.154 | -0.127 | 0.092 |
| 42 | 0.067 | 0.026 | -0.028 |
| 43 | -0.099 | -0.075 | 0.238 |
| | | | |

| 44 | -0.023 | 0.006 | 0.106 |
|----|--------|--------|--------|
| 45 | 0.312 | 0.330 | -0.352 |
| 46 | 0.087 | -0.046 | -0.010 |
| 47 | -0.007 | 0.035 | 0.065 |
| 48 | 0.341 | -0.027 | -0.287 |
| 49 | 0.329 | -0.109 | 0.146 |
| 50 | -0.009 | 0.024 | -0.014 |

Table A.7. Factor Loadings for Listening-Low Proficiency

| Item | Factor Loadings | | | | |
|------|-----------------|--------|--------|--|--|
| | 1 | 2 | 3 | | |
| 1 | 0.398 | -0.273 | -0.173 | | |
| 2 | 0.056 | -0.145 | 0.212 | | |
| 3 | 0.575 | -0.169 | 0.204 | | |
| 4 | 0.133 | 0.148 | -0.068 | | |
| 5 | 0.143 | -0.096 | 0.262 | | |
| 6 | 0.425 | -0.348 | 0.079 | | |
| 7 | 0.444 | -0.264 | 0.009 | | |
| 8 | 0.269 | 0.025 | 0.201 | | |
| 9 | 0.165 | -0.210 | 0.276 | | |
| 10 | 0.139 | -0.141 | -0.153 | | |
| 11 | 0.142 | 0.067 | 0.378 | | |
| 12 | 0.529 | -0.063 | -0.179 | | |
| 13 | 0.085 | -0.110 | -0.186 | | |
| 14 | 0.183 | 0.242 | 0.189 | | |
| 15 | 0.266 | 0.013 | 0.260 | | |
| 16 | 0.636 | -0.058 | 0.168 | | |
| 17 | 0.524 | 0.036 | 0.180 | | |
| 18 | 0.552 | 0.089 | 0.080 | | |
| 19 | 0.473 | 0.035 | -0.052 | | |
| 20 | 0.449 | 0.060 | 0.036 | | |
| 21 | 0.216 | -0.166 | -0.314 | | |
| 22 | 0.579 | -0.024 | -0.080 | | |
| 23 | 0.564 | -0.090 | 0.002 | | |
| 24 | 0.316 | 0.173 | -0.220 | | |
| 25 | 0.293 | 0.122 | 0.017 | | |
| 26 | 0.405 | 0.028 | 0.023 | | |
| 27 | 0.168 | -0.074 | 0.124 | | |
| 28 | 0.617 | 0.064 | -0.173 | | |
| 29 | 0.601 | -0.094 | 0.020 | | |
| 30 | 0.134 | -0.156 | 0.004 | | |
| 31 | 0.231 | 0.079 | 0.228 | | |
| 32 | 0.485 | -0.046 | -0.175 | | |
| 33 | 0.136 | 0.000 | -0.062 | | |
| 34 | 0.064 | 0.093 | -0.168 | | |
| 35 | 0.182 | 0.113 | 0.085 | | |

| 36 | 0.446 | 0.324 | 0.071 |
|----|--------|--------|--------|
| 37 | 0.011 | 0.238 | -0.032 |
| 38 | 0.088 | 0.074 | 0.139 |
| 39 | -0.037 | 0.134 | -0.004 |
| 40 | 0.139 | -0.173 | -0.288 |
| 41 | 0.076 | 0.354 | 0.125 |
| 42 | 0.056 | 0.288 | -0.071 |
| 43 | 0.361 | 0.295 | -0.325 |
| 44 | 0.234 | 0.254 | -0.227 |
| 45 | 0.322 | 0.439 | 0.045 |
| 46 | -0.066 | 0.268 | 0.202 |
| 47 | 0.035 | 0.247 | -0.158 |
| 48 | 0.069 | 0.105 | -0.148 |
| 49 | -0.190 | 0.114 | 0.191 |
| 50 | 0.044 | 0.139 | 0.014 |

Appendix B

40

0.585

-0.171

0.092

0.176

Factor Loadings for Form EE-GCVR

Table B.1. Factor Loadings for GCVR -All Examinees

| Examin | iees | | | | 41 | 0.431 | 0.177 | 0.031 | -0.163 |
|--------|--------|----------|---------|--------|----|-------|--------|--------|--------|
| Item | | Factor L | oadings | | 42 | 0.554 | 0.017 | 0.038 | -0.045 |
| | 1 | 2 | 3 | 4 | 43 | 0.319 | 0.135 | 0.106 | 0.133 |
| 1 | 0.553 | -0.127 | 0.261 | 0.107 | 44 | 0.343 | 0.224 | 0.104 | -0.015 |
| 2 | 0.598 | 0.099 | -0.012 | -0.134 | 45 | 0.274 | 0.189 | -0.001 | -0.052 |
| 3 | 0.625 | 0.076 | 0.089 | -0.002 | 46 | 0.365 | -0.159 | 0.038 | -0.120 |
| 4 | 0.629 | -0.123 | 0.138 | -0.101 | 47 | 0.430 | 0.309 | -0.020 | -0.039 |
| 5 | 0.382 | -0.008 | 0.162 | 0.106 | 48 | 0.258 | 0.369 | 0.130 | 0.085 |
| 6 | 0.699 | -0.028 | 0.186 | -0.154 | 49 | 0.675 | -0.010 | 0.180 | -0.164 |
| 7 | 0.242 | 0.290 | -0.003 | -0.019 | 50 | 0.277 | 0.209 | 0.146 | 0.111 |
| 8 | 0.720 | -0.033 | 0.257 | 0.032 | 51 | 0.716 | -0.237 | -0.235 | -0.138 |
| 9 | 0.323 | 0.281 | -0.012 | -0.085 | 52 | 0.580 | -0.389 | -0.308 | -0.088 |
| 10 | 0.457 | 0.346 | -0.219 | -0.177 | 53 | 0.567 | -0.104 | -0.257 | -0.062 |
| 11 | 0.649 | -0.194 | 0.168 | 0.020 | 54 | 0.607 | -0.163 | -0.094 | -0.102 |
| 12 | 0.544 | 0.099 | 0.245 | -0.140 | 55 | 0.478 | 0.193 | -0.377 | -0.259 |
| 13 | 0.593 | -0.216 | 0.085 | -0.032 | 56 | 0.501 | -0.087 | -0.085 | -0.115 |
| 14 | 0.268 | 0.503 | 0.060 | -0.177 | 57 | 0.675 | -0.522 | 0.112 | 0.030 |
| 15 | 0.631 | -0.069 | -0.104 | 0.168 | 58 | 0.641 | -0.316 | -0.056 | 0.137 |
| 16 | 0.532 | 0.190 | -0.057 | -0.262 | 59 | 0.743 | -0.255 | 0.013 | 0.006 |
| 17 | 0.068 | 0.262 | 0.220 | 0.202 | 60 | 0.554 | -0.183 | -0.095 | -0.186 |
| 18 | 0.316 | -0.243 | 0.343 | 0.488 | 61 | 0.637 | -0.377 | -0.098 | -0.113 |
| 19 | 0.026 | 0.628 | -0.058 | -0.091 | 62 | 0.470 | 0.276 | 0.153 | -0.080 |
| 20 | 0.203 | 0.171 | -0.075 | 0.128 | 63 | 0.382 | 0.070 | 0.046 | -0.048 |
| 21 | 0.401 | 0.066 | 0.160 | 0.150 | 64 | 0.631 | -0.309 | -0.304 | 0.048 |
| 22 | 0.482 | 0.192 | -0.007 | -0.077 | 65 | 0.599 | -0.145 | -0.030 | 0.019 |
| 23 | 0.718 | 0.332 | 0.164 | -0.080 | 66 | 0.435 | 0.103 | -0.153 | -0.005 |
| 24 | 0.546 | 0.281 | 0.022 | -0.162 | 67 | 0.683 | -0.196 | -0.182 | -0.001 |
| 25 | 0.618 | -0.107 | 0.129 | -0.098 | 68 | 0.651 | -0.353 | 0.103 | 0.027 |
| 26 | 0.668 | -0.161 | -0.007 | -0.265 | 69 | 0.444 | 0.165 | 0.009 | 0.077 |
| 27 | 0.585 | 0.265 | 0.371 | -0.110 | 70 | 0.736 | -0.263 | -0.042 | -0.106 |
| 28 | 0.683 | 0.090 | 0.123 | -0.017 | 71 | 0.610 | 0.034 | -0.046 | -0.085 |
| 29 | 0.559 | 0.165 | 0.188 | 0.015 | 72 | 0.617 | -0.085 | 0.143 | 0.009 |
| 30 | 0.492 | 0.434 | -0.189 | -0.183 | 73 | 0.642 | -0.287 | 0.172 | -0.009 |
| 31 | 0.448 | 0.406 | 0.115 | -0.254 | 74 | 0.570 | 0.001 | 0.151 | 0.042 |
| 32 | 0.477 | -0.059 | -0.206 | -0.055 | 75 | 0.756 | -0.329 | -0.020 | -0.026 |
| 33 | 0.228 | 0.040 | 0.222 | 0.088 | 76 | 0.719 | -0.308 | -0.178 | 0.137 |
| 34 | 0.545 | 0.172 | 0.136 | 0.001 | 77 | 0.566 | -0.175 | -0.018 | 0.077 |
| 35 | -0.009 | 0.342 | 0.242 | 0.005 | 78 | 0.633 | -0.471 | 0.192 | 0.011 |
| 36 | 0.325 | 0.198 | -0.091 | 0.002 | 79 | 0.400 | 0.018 | 0.130 | 0.163 |
| 37 | -0.144 | 0.164 | 0.146 | 0.060 | 80 | 0.604 | -0.126 | 0.027 | -0.007 |
| 38 | 0.476 | 0.298 | 0.107 | -0.124 | 81 | 0.436 | 0.184 | -0.038 | 0.190 |
| 39 | 0.251 | 0.371 | -0.013 | -0.249 | 82 | 0.421 | 0.160 | -0.182 | 0.125 |

| 83 | 0.386 | 0.213 | -0.255 | 0.319 | 25 | 0.602 | -0.053 | -0.186 |
|-----|-------|--------|--------|--------|----|--------|--------|--------|
| 84 | 0.351 | 0.232 | -0.228 | 0.279 | 26 | 0.704 | -0.105 | -0.070 |
| 85 | 0.384 | 0.334 | 0.023 | 0.200 | 27 | 0.605 | 0.264 | -0.407 |
| 86 | 0.696 | -0.169 | -0.154 | 0.019 | 28 | 0.683 | 0.071 | -0.129 |
| 87 | 0.393 | 0.189 | -0.087 | 0.158 | 29 | 0.549 | 0.138 | -0.192 |
| 88 | 0.511 | 0.329 | -0.124 | 0.077 | 30 | 0.459 | 0.459 | 0.194 |
| 89 | 0.593 | -0.066 | -0.155 | 0.168 | 31 | 0.388 | 0.470 | -0.153 |
| 90 | 0.420 | 0.384 | -0.043 | 0.251 | 32 | 0.437 | -0.027 | 0.132 |
| 91 | 0.312 | 0.268 | -0.128 | 0.261 | 33 | 0.188 | 0.026 | -0.207 |
| 92 | 0.406 | 0.192 | -0.067 | 0.273 | 34 | 0.536 | 0.135 | -0.104 |
| 93 | 0.572 | -0.038 | -0.203 | 0.240 | 35 | 0.015 | 0.316 | -0.209 |
| 94 | 0.407 | 0.336 | -0.079 | 0.275 | 36 | 0.342 | 0.209 | 0.136 |
| 95 | 0.227 | 0.255 | -0.134 | 0.079 | 37 | -0.191 | 0.117 | -0.104 |
| 96 | 0.498 | 0.197 | -0.163 | 0.116 | 38 | 0.436 | 0.366 | -0.171 |
| 97 | 0.084 | 0.275 | -0.155 | -0.015 | 39 | 0.242 | 0.462 | -0.061 |
| 98 | 0.435 | 0.085 | -0.173 | 0.040 | 40 | 0.574 | -0.213 | -0.089 |
| 99 | 0.372 | 0.246 | -0.198 | 0.179 | 41 | 0.447 | 0.158 | -0.048 |
| 100 | 0.565 | 0.093 | 0.002 | 0.157 | 42 | 0.531 | 0.026 | -0.071 |
| | | | | | 43 | 0.303 | 0.108 | -0.052 |

-0.007 -0.238 -0.032 0.020 0.095 -0.179 -0.314 -0.131 0.137 0.024 -0.031 0.012 0.049 -0.098 -0.267 0.140 -0.095 -0.080

0.215

-0.001

-0.126

Table B.2. Factor Loadings for GCVR-Female

| | | | | _ | - | - | | |
|-------|---|---|---|--|-------------------|---|--|--------|
| | Factor L | oadings | | 46 | 0.379 | -0.142 | -0.063 | -0.115 |
| 1 | | | 4 | 47 | 0.416 | 0.334 | -0.012 | -0.011 |
| 0.543 | -0.158 | -0.281 | 0.148 | 48 | 0.305 | 0.302 | -0.070 | 0.112 |
| 0.580 | 0.081 | 0.003 | -0.152 | 49 | 0.685 | -0.002 | -0.209 | -0.076 |
| 0.608 | | | -0.029 | 50 | 0.226 | 0.172 | -0.161 | 0.156 |
| 0.615 | -0.124 | -0.248 | -0.034 | 51 | 0.691 | -0.242 | 0.276 | -0.182 |
| 0.375 | -0.005 | -0.143 | 0.131 | 52 | 0.599 | -0.362 | 0.327 | -0.135 |
| 0.665 | 0.005 | -0.252 | -0.131 | 53 | 0.526 | -0.042 | 0.287 | -0.155 |
| 0.277 | 0.327 | -0.012 | -0.045 | 54 | 0.566 | -0.147 | 0.168 | -0.186 |
| 0.732 | -0.106 | -0.241 | 0.092 | 55 | 0.456 | 0.227 | 0.285 | -0.192 |
| 0.332 | 0.260 | -0.001 | -0.121 | 56 | 0.492 | -0.085 | 0.101 | -0.174 |
| 0.427 | 0.373 | 0.250 | -0.219 | 57 | 0.647 | -0.548 | -0.084 | -0.005 |
| 0.612 | -0.206 | -0.220 | 0.046 | 58 | 0.603 | -0.373 | 0.138 | 0.073 |
| 0.554 | 0.101 | -0.333 | -0.053 | 59 | 0.708 | -0.251 | 0.012 | 0.010 |
| 0.598 | -0.229 | -0.140 | -0.050 | 60 | 0.539 | -0.132 | 0.064 | -0.253 |
| 0.300 | 0.483 | -0.085 | -0.155 | 61 | 0.671 | -0.344 | 0.078 | -0.151 |
| 0.603 | -0.092 | 0.091 | 0.145 | 62 | 0.453 | 0.241 | -0.115 | -0.107 |
| 0.564 | 0.157 | 0.035 | -0.265 | 63 | 0.377 | 0.074 | -0.002 | -0.072 |
| 0.090 | 0.236 | -0.149 | 0.255 | 64 | 0.596 | -0.348 | 0.428 | 0.018 |
| 0.343 | -0.318 | -0.103 | 0.414 | 65 | 0.599 | -0.181 | 0.077 | -0.005 |
| 0.046 | 0.615 | 0.079 | -0.101 | 66 | 0.454 | 0.114 | 0.172 | -0.055 |
| 0.206 | 0.165 | 0.137 | 0.150 | 67 | 0.653 | -0.170 | 0.218 | -0.088 |
| 0.412 | 0.001 | -0.065 | 0.184 | 68 | 0.606 | -0.378 | -0.133 | -0.018 |
| 0.478 | 0.178 | 0.095 | -0.083 | 69 | 0.455 | 0.165 | 0.005 | 0.051 |
| 0.689 | 0.328 | -0.195 | -0.032 | 70 | 0.712 | -0.208 | 0.046 | -0.102 |
| 0.547 | 0.291 | -0.054 | -0.114 | 71 | 0.607 | 0.040 | 0.079 | -0.034 |
| | | | | 72 | 0.594 | -0.089 | -0.173 | 0.083 |
| | 0.543 0.580 0.608 0.615 0.375 0.665 0.277 0.732 0.332 0.427 0.612 0.554 0.598 0.300 0.603 0.564 0.090 0.343 0.046 0.206 0.412 0.478 0.689 | 1 2 0.543 -0.158 0.580 0.081 0.608 0.068 0.615 -0.124 0.375 -0.005 0.665 0.005 0.277 0.327 0.732 -0.106 0.332 0.260 0.427 0.373 0.612 -0.206 0.554 0.101 0.598 -0.229 0.300 0.483 0.603 -0.092 0.564 0.157 0.090 0.236 0.343 -0.318 0.046 0.615 0.206 0.165 0.412 0.001 0.478 0.178 0.689 0.328 | 0.543 -0.158 -0.281 0.580 0.081 0.003 0.608 0.068 -0.093 0.615 -0.124 -0.248 0.375 -0.005 -0.143 0.665 0.005 -0.252 0.277 0.327 -0.012 0.732 -0.106 -0.241 0.332 0.260 -0.001 0.427 0.373 0.250 0.612 -0.206 -0.220 0.554 0.101 -0.333 0.598 -0.229 -0.140 0.300 0.483 -0.085 0.603 -0.092 0.091 0.564 0.157 0.035 0.090 0.236 -0.149 0.343 -0.318 -0.103 0.046 0.615 0.079 0.206 0.165 0.137 0.412 0.001 -0.065 0.478 0.178 0.095 0.689 0.328 -0.195 </td <td>1 2 3 4 0.543 -0.158 -0.281 0.148 0.580 0.081 0.003 -0.152 0.608 0.068 -0.093 -0.029 0.615 -0.124 -0.248 -0.034 0.375 -0.005 -0.143 0.131 0.665 0.005 -0.252 -0.131 0.277 0.327 -0.012 -0.045 0.732 -0.106 -0.241 0.092 0.332 0.260 -0.001 -0.121 0.427 0.373 0.250 -0.219 0.612 -0.206 -0.220 0.046 0.554 0.101 -0.333 -0.053 0.598 -0.229 -0.140 -0.050 0.300 0.483 -0.085 -0.155 0.603 -0.092 0.091 0.145 0.564 0.157 0.035 -0.265 0.090 0.236 -0.149 0.255 0.343</td> <td>1 2 3 4 47 0.543</td> <td>1 2 3 4 47 0.416 0.543 -0.158 -0.281 0.148 48 0.305 0.580 0.081 0.003 -0.152 49 0.685 0.608 0.068 -0.093 -0.029 50 0.226 0.615 -0.124 -0.248 -0.034 51 0.691 0.375 -0.005 -0.143 0.131 52 0.599 0.665 0.005 -0.252 -0.131 53 0.526 0.277 0.327 -0.012 -0.045 54 0.566 0.732 -0.106 -0.241 0.092 55 0.456 0.332 0.260 -0.001 -0.121 56 0.492 0.427 0.373 0.250 -0.219 57 0.647 0.612 -0.206 -0.220 0.046 58 0.603 0.554 0.101 -0.333 -0.053 59 0.708 0.598</td> <td>1 2 3 4 47 0.416 0.334 0.543 -0.158 -0.281 0.148 48 0.305 0.302 0.580 0.081 0.003 -0.152 49 0.685 -0.002 0.608 0.068 -0.093 -0.029 50 0.226 0.172 0.615 -0.124 -0.248 -0.034 51 0.691 -0.242 0.375 -0.005 -0.143 0.131 52 0.599 -0.362 0.665 0.005 -0.252 -0.131 53 0.526 -0.042 0.277 0.327 -0.012 -0.045 54 0.566 -0.147 0.732 -0.106 -0.241 0.092 55 0.456 0.227 0.332 0.260 -0.001 -0.121 56 0.492 -0.085 0.427 0.373 0.250 -0.219 57 0.647 -0.548 0.612 -0.206 -0.220</td> <td> 1</td> | 1 2 3 4 0.543 -0.158 -0.281 0.148 0.580 0.081 0.003 -0.152 0.608 0.068 -0.093 -0.029 0.615 -0.124 -0.248 -0.034 0.375 -0.005 -0.143 0.131 0.665 0.005 -0.252 -0.131 0.277 0.327 -0.012 -0.045 0.732 -0.106 -0.241 0.092 0.332 0.260 -0.001 -0.121 0.427 0.373 0.250 -0.219 0.612 -0.206 -0.220 0.046 0.554 0.101 -0.333 -0.053 0.598 -0.229 -0.140 -0.050 0.300 0.483 -0.085 -0.155 0.603 -0.092 0.091 0.145 0.564 0.157 0.035 -0.265 0.090 0.236 -0.149 0.255 0.343 | 1 2 3 4 47 0.543 | 1 2 3 4 47 0.416 0.543 -0.158 -0.281 0.148 48 0.305 0.580 0.081 0.003 -0.152 49 0.685 0.608 0.068 -0.093 -0.029 50 0.226 0.615 -0.124 -0.248 -0.034 51 0.691 0.375 -0.005 -0.143 0.131 52 0.599 0.665 0.005 -0.252 -0.131 53 0.526 0.277 0.327 -0.012 -0.045 54 0.566 0.732 -0.106 -0.241 0.092 55 0.456 0.332 0.260 -0.001 -0.121 56 0.492 0.427 0.373 0.250 -0.219 57 0.647 0.612 -0.206 -0.220 0.046 58 0.603 0.554 0.101 -0.333 -0.053 59 0.708 0.598 | 1 2 3 4 47 0.416 0.334 0.543 -0.158 -0.281 0.148 48 0.305 0.302 0.580 0.081 0.003 -0.152 49 0.685 -0.002 0.608 0.068 -0.093 -0.029 50 0.226 0.172 0.615 -0.124 -0.248 -0.034 51 0.691 -0.242 0.375 -0.005 -0.143 0.131 52 0.599 -0.362 0.665 0.005 -0.252 -0.131 53 0.526 -0.042 0.277 0.327 -0.012 -0.045 54 0.566 -0.147 0.732 -0.106 -0.241 0.092 55 0.456 0.227 0.332 0.260 -0.001 -0.121 56 0.492 -0.085 0.427 0.373 0.250 -0.219 57 0.647 -0.548 0.612 -0.206 -0.220 | 1 |

44

45

0.375

0.274

0.227

0.244

-0.122

0.004

| 73 | 0.631 | -0.356 | -0.205 | -0.023 | 16 | 0.450 | 0.268 | 0.150 | -0.175 |
|-----|-------|--------|--------|--------|----|--------|--------|--------|--------|
| 74 | 0.598 | -0.026 | -0.091 | 0.063 | 17 | 0.061 | 0.262 | -0.008 | -0.090 |
| 75 | 0.760 | -0.346 | 0.025 | -0.052 | 18 | 0.384 | 0.278 | -1.207 | 0.049 |
| 76 | 0.668 | -0.359 | 0.299 | 0.083 | 19 | 0.021 | 0.592 | 0.203 | 0.089 |
| 77 | 0.512 | -0.224 | 0.083 | 0.080 | 20 | 0.210 | 0.126 | 0.192 | -0.014 |
| 78 | 0.608 | -0.536 | -0.213 | 0.056 | 21 | 0.388 | 0.245 | -0.108 | -0.065 |
| 79 | 0.408 | -0.007 | -0.032 | 0.187 | 22 | 0.503 | 0.270 | -0.080 | -0.315 |
| 80 | 0.623 | -0.124 | -0.024 | 0.014 | 23 | 0.819 | 0.387 | -0.224 | -0.019 |
| 81 | 0.373 | 0.203 | 0.028 | 0.242 | 24 | 0.541 | 0.259 | 0.130 | -0.138 |
| 82 | 0.387 | 0.182 | 0.192 | 0.103 | 25 | 0.644 | -0.293 | 0.118 | -0.250 |
| 83 | 0.380 | 0.227 | 0.330 | 0.265 | 26 | 0.584 | -0.235 | 0.115 | -0.215 |
| 84 | 0.334 | 0.222 | 0.287 | 0.296 | 27 | 0.559 | 0.242 | -0.015 | -0.300 |
| 85 | 0.431 | 0.304 | 0.002 | 0.166 | 28 | 0.687 | 0.178 | 0.003 | -0.155 |
| 86 | 0.673 | -0.132 | 0.136 | 0.061 | 29 | 0.571 | 0.212 | 0.365 | -0.097 |
| 87 | 0.407 | 0.163 | 0.108 | 0.153 | 30 | 0.574 | 0.431 | 0.235 | -0.149 |
| 88 | 0.456 | 0.374 | 0.073 | 0.052 | 31 | 0.645 | 0.291 | -0.317 | -0.316 |
| 89 | 0.558 | 0.028 | 0.195 | 0.243 | 32 | 0.570 | -0.145 | 0.008 | 0.225 |
| 90 | 0.393 | 0.358 | 0.052 | 0.284 | 33 | 0.355 | 0.059 | -0.095 | -0.011 |
| 91 | 0.244 | 0.310 | 0.079 | 0.253 | 34 | 0.613 | 0.205 | 0.023 | -0.068 |
| 92 | 0.354 | 0.216 | 0.081 | 0.266 | 35 | -0.052 | 0.381 | -0.181 | 0.041 |
| 93 | 0.510 | 0.041 | 0.168 | 0.262 | 36 | 0.304 | 0.094 | 0.067 | -0.087 |
| 94 | 0.347 | 0.392 | 0.036 | 0.261 | 37 | 0.010 | 0.226 | -0.072 | -0.054 |
| 95 | 0.179 | 0.295 | 0.077 | 0.065 | 38 | 0.584 | 0.056 | 0.011 | 0.032 |
| 96 | 0.464 | 0.207 | 0.162 | 0.041 | 39 | 0.289 | 0.038 | -0.013 | -0.047 |
| 97 | 0.122 | 0.275 | 0.152 | -0.054 | 40 | 0.685 | -0.154 | -0.071 | 0.227 |
| 98 | 0.382 | 0.108 | 0.142 | 0.037 | 41 | 0.400 | 0.172 | 0.179 | -0.222 |
| 99 | 0.378 | 0.204 | 0.218 | 0.169 | 42 | 0.620 | 0.010 | 0.048 | 0.027 |
| 100 | 0.545 | 0.072 | -0.024 | 0.199 | 43 | 0.379 | 0.180 | 0.248 | -0.157 |
| | | | | | 44 | 0.267 | 0.094 | 0.137 | 0.182 |
| | | | | | | | | | |

Table B.3. Factor Loadings for GCVR-Male

| Table B | 3.3. Factor | r Loadings | for GCV | R-Male | 45 | 0.282 | 0.050 | -0.114 | 0.089 |
|---------|-------------|------------|---------|--------|----|-------|--------|--------|--------|
| Item | | Factor L | oadings | | 46 | 0.320 | -0.187 | -0.055 | -0.054 |
| | 1 | 2 | 3 | 4 | 47 | 0.474 | 0.238 | 0.142 | -0.044 |
| 1 | 0.587 | -0.014 | -0.171 | 0.059 | 48 | 0.179 | 0.522 | -0.051 | 0.077 |
| 2 | 0.639 | 0.170 | 0.177 | -0.106 | 49 | 0.654 | -0.082 | 0.066 | -0.295 |
| 3 | 0.676 | 0.126 | -0.038 | 0.011 | 50 | 0.423 | 0.266 | 0.147 | -0.092 |
| 4 | 0.648 | -0.103 | 0.074 | -0.046 | 51 | 0.745 | -0.219 | 0.076 | -0.206 |
| 5 | 0.408 | -0.045 | -0.123 | -0.035 | 52 | 0.525 | -0.410 | 0.009 | -0.008 |
| 6 | 0.786 | -0.112 | -0.076 | -0.079 | 53 | 0.643 | -0.273 | 0.080 | 0.074 |
| 7 | 0.157 | 0.138 | -0.116 | 0.106 | 54 | 0.702 | -0.179 | -0.033 | 0.059 |
| 8 | 0.704 | 0.131 | -0.034 | -0.123 | 55 | 0.552 | 0.044 | 0.084 | 0.022 |
| 9 | 0.289 | 0.375 | 0.173 | 0.091 | 56 | 0.530 | -0.084 | -0.103 | 0.116 |
| 10 | 0.541 | 0.460 | -0.363 | -0.149 | 57 | 0.728 | -0.457 | -0.201 | -0.055 |
| 11 | 0.742 | -0.089 | 0.028 | -0.148 | 58 | 0.732 | -0.183 | -0.056 | 0.109 |
| 12 | 0.516 | 0.101 | 0.115 | -0.003 | 59 | 0.802 | -0.239 | 0.036 | -0.074 |
| 13 | 0.582 | -0.190 | 0.018 | -0.042 | 60 | 0.581 | -0.326 | 0.006 | 0.096 |
| 14 | 0.187 | 0.543 | 0.192 | -0.200 | 61 | 0.549 | -0.473 | -0.086 | 0.045 |
| 15 | 0.694 | -0.020 | 0.169 | 0.157 | 62 | 0.526 | 0.409 | -0.117 | -0.149 |
| | | | | | 63 | 0.381 | 0.139 | -0.142 | -0.114 |

| 64 | 0.687 | -0.175 | 0.095 | -0.120 | 6 | 0.611 | -0.127 | 0.059 | -0.043 |
|-----|-------|--------|--------|--------|----|--------|--------|--------|--------|
| 65 | 0.605 | -0.026 | -0.071 | 0.179 | 7 | 0.294 | 0.032 | -0.279 | -0.228 |
| 66 | 0.396 | -0.063 | 0.206 | 0.137 | 8 | 0.708 | -0.062 | 0.116 | -0.087 |
| 67 | 0.735 | -0.267 | -0.194 | 0.173 | 9 | 0.384 | 0.389 | -0.033 | -0.043 |
| 68 | 0.763 | -0.300 | -0.091 | 0.118 | 10 | 0.508 | -0.040 | -0.193 | -0.458 |
| 69 | 0.438 | 0.078 | -0.035 | 0.292 | 11 | 0.471 | -0.139 | 0.149 | -0.012 |
| 70 | 0.775 | -0.365 | 0.015 | -0.102 | 12 | 0.533 | -0.099 | 0.019 | -0.054 |
| 71 | 0.617 | 0.055 | -0.053 | -0.231 | 13 | 0.471 | -0.008 | 0.146 | -0.234 |
| 72 | 0.697 | -0.197 | 0.127 | -0.223 | 14 | 0.519 | 0.336 | -0.280 | 0.032 |
| 73 | 0.696 | -0.106 | 0.079 | -0.161 | 15 | 0.521 | -0.192 | 0.011 | -0.032 |
| 74 | 0.491 | 0.149 | -0.083 | -0.079 | 16 | 0.516 | -0.057 | -0.029 | -0.053 |
| 75 | 0.748 | -0.325 | -0.035 | 0.008 | 17 | 0.266 | 0.208 | 0.087 | 0.089 |
| 76 | 0.793 | -0.158 | 0.028 | 0.006 | 18 | 0.357 | 0.066 | -0.573 | -1.042 |
| 77 | 0.676 | 0.034 | 0.062 | -0.102 | 19 | 0.348 | 0.377 | -0.197 | 0.056 |
| 78 | 0.679 | -0.322 | 0.017 | -0.066 | 20 | 0.242 | -0.010 | 0.186 | -0.014 |
| 79 | 0.411 | 0.106 | -0.456 | -0.205 | 21 | 0.303 | -0.004 | 0.091 | -0.078 |
| 80 | 0.572 | -0.248 | 0.049 | 0.031 | 22 | 0.356 | -0.147 | -0.055 | -0.176 |
| 81 | 0.602 | 0.118 | 0.067 | -0.005 | 23 | 0.927 | 0.025 | -0.084 | -0.149 |
| 82 | 0.503 | 0.135 | 0.028 | 0.195 | 24 | 0.685 | 0.183 | 0.016 | 0.018 |
| 83 | 0.409 | 0.112 | 0.051 | 0.292 | 25 | 0.500 | -0.368 | -0.345 | -0.006 |
| 84 | 0.430 | 0.174 | 0.261 | 0.203 | 26 | 0.600 | -0.152 | 0.148 | 0.052 |
| 85 | 0.334 | 0.200 | 0.335 | 0.245 | 27 | 0.611 | -0.151 | -0.014 | -0.031 |
| 86 | 0.751 | -0.254 | 0.249 | 0.051 | 28 | 0.732 | -0.206 | 0.111 | -0.235 |
| 87 | 0.374 | 0.190 | -0.017 | 0.301 | 29 | 0.565 | -0.194 | 0.041 | -0.013 |
| 88 | 0.686 | 0.222 | -0.259 | 0.270 | 30 | 0.701 | -0.055 | 0.106 | -0.230 |
| 89 | 0.656 | -0.230 | -0.232 | 0.034 | 31 | 0.708 | 0.389 | 0.086 | -0.079 |
| 90 | 0.504 | 0.322 | 0.165 | 0.154 | 32 | 0.253 | -0.195 | -0.337 | 0.371 |
| 91 | 0.471 | 0.181 | -0.005 | 0.365 | 33 | 0.123 | 0.076 | -0.396 | -0.232 |
| 92 | 0.535 | 0.126 | -0.081 | 0.329 | 34 | 0.616 | -0.013 | -0.045 | -0.308 |
| 93 | 0.687 | -0.239 | 0.026 | 0.297 | 35 | 0.014 | 0.605 | -0.204 | -0.049 |
| 94 | 0.575 | 0.116 | -0.073 | 0.311 | 36 | 0.343 | 0.105 | -0.070 | 0.228 |
| 95 | 0.349 | 0.191 | 0.069 | 0.160 | 37 | -0.200 | -0.001 | -0.066 | -0.003 |
| 96 | 0.604 | 0.181 | -0.029 | 0.307 | 38 | 0.594 | 0.216 | -0.092 | 0.122 |
| 97 | 0.002 | 0.236 | 0.128 | 0.241 | 39 | 0.370 | 0.364 | -0.132 | 0.169 |
| 98 | 0.552 | 0.123 | 0.045 | 0.030 | 40 | 0.284 | 0.006 | 0.126 | 0.024 |
| 99 | 0.371 | 0.336 | 0.084 | 0.298 | 41 | 0.504 | -0.074 | 0.145 | -0.118 |
| 100 | 0.647 | 0.060 | 0.219 | 0.117 | 42 | 0.468 | 0.074 | 0.032 | 0.250 |
| | | | | | 43 | 0.357 | 0.019 | 0.043 | 0.051 |

Table B.4. Factor Loadings for GCVR-Tagalog/Filipino

| Item | | 46 | | | |
|------|-------|--------|--------|--------|----|
| | 1 | 2 | 3 | 4 | 47 |
| 1 | 0.434 | -0.102 | 0.015 | -0.089 | 48 |
| 2 | 0.534 | -0.047 | -0.015 | -0.048 | 49 |
| 3 | 0.506 | -0.203 | 0.076 | -0.051 | 50 |
| 4 | 0.503 | -0.163 | 0.161 | -0.094 | 51 |
| 5 | 0.237 | 0.083 | 0.051 | -0.037 | 52 |
| | | | | | F2 |

| | 54 | 0.459 | 0.088 | -0.519 | 0.010 | Table | B.5. Fact | tor Loadi | ngs for | GCVR- |
|--|-----|-------|--------|--------|--------|-------|-----------|-----------|---------------|--------|
| Teach Factor Loadings Fa | | | | | | | | | \mathcal{C} | |
| 57 | 56 | 0.349 | 0.159 | -0.057 | -0.183 | | | Factor L | oadings | |
| 68 0.574 -0.103 -0.046 0.291 1 0.230 0.566 0.165 -0.165 59 0.550 -0.285 -0.219 0.178 2 0.644 0.022 0.131 0.46 60 0.388 0.013 0.080 -0.152 3 0.466 0.184 -0.028 -0.24 61 0.363 -0.223 -0.602 0.211 4 0.477 0.289 0.031 0.03 62 0.645 0.211 -0.082 0.028 5 0.137 -0.048 0.001 0.19 63 0.310 0.171 0.057 0.100 6 0.454 0.316 0.300 -0.05 64 0.133 0.658 1.339 0.104 7 0.309 0.289 -0.035 0.15 66 0.384 -0.170 0.023 0.121 8 0.692 0.003 0.488 0.54 67 0.510 -0.088 0.221 | 57 | 0.654 | 1.131 | -0.367 | 0.677 | | 1 | | | 4 |
| 59 | 58 | 0.574 | -0.103 | -0.046 | 0.291 | 1 | 0.230 | | | -0.187 |
| 61 0.363 -0.223 -0.602 0.211 | 59 | 0.550 | -0.285 | -0.219 | 0.178 | 2 | | 0.022 | 0.131 | 0.145 |
| 62 0.645 0.211 -0.082 0.028 5 0.137 -0.048 0.001 0.19 63 0.310 0.171 0.057 0.100 6 0.454 0.316 0.300 -0.02 64 0.133 0.658 1.330 -0.104 7 0.309 0.288 -0.035 0.15 65 0.348 0.170 0.208 -0.121 8 0.692 0.003 0.488 0.54 66 0.384 -0.092 0.123 0.101 9 0.531 -0.053 -0.014 0.17 67 0.510 -0.088 0.291 0.380 10 0.588 0.023 -0.101 -0.06 68 0.120 -0.047 -0.259 0.436 11 0.434 0.617 -0.118 -0.11 0.434 0.617 -0.118 -0.11 0.444 0.617 -0.018 14 0.161 0.026 0.214 0.027 0.44 0.227 0.33 | 60 | 0.388 | 0.013 | 0.080 | -0.152 | | 0.466 | 0.184 | | -0.240 |
| 63 0.310 0.171 0.057 0.100 6 0.454 0.316 0.300 -0.02 64 0.133 0.668 1.330 -0.104 7 0.309 0.289 -0.035 0.15 65 0.348 0.170 0.208 -0.121 8 0.692 0.003 0.488 0.54 66 0.384 -0.092 0.123 0.101 9 0.531 -0.053 -0.014 0.17 67 0.510 -0.088 0.291 0.380 10 0.588 0.023 -0.014 0.01 68 0.120 -0.047 -0.259 0.436 11 0.434 0.617 -0.108 -0.00 69 0.494 -0.153 0.071 0.018 14 0.161 0.076 -0.214 -0.21 71 0.637 -0.323 0.158 0.073 13 0.280 0.276 -0.227 0.39 72 0.626 -0.221 0.010< | 61 | 0.363 | -0.223 | -0.602 | 0.211 | 4 | 0.477 | 0.289 | 0.031 | 0.034 |
| 64 0.133 0.658 1.330 -0.104 7 0.309 0.289 -0.035 0.15 65 0.348 0.170 0.208 -0.121 8 0.692 0.003 0.488 0.54 66 0.348 -0.092 0.123 0.101 9 0.531 -0.053 -0.014 0.17 67 0.510 -0.088 0.291 0.380 10 0.588 0.023 -0.101 -0.06 68 0.120 -0.047 -0.259 0.436 11 0.434 0.617 -0.108 -0.00 69 0.494 -0.153 0.071 -0.010 12 0.338 0.570 0.118 -0.11 70 0.637 -0.323 0.158 0.073 13 0.280 0.276 -0.214 -0.21 71 0.635 -0.246 0.107 0.018 14 0.161 0.076 0.322 0.113 0.16 73 0.462 0.03 | 62 | 0.645 | 0.211 | -0.082 | 0.028 | 5 | 0.137 | -0.048 | 0.001 | 0.190 |
| 65 0.348 0.170 0.208 -0.121 8 0.692 0.003 0.488 0.54 66 0.334 -0.092 0.123 0.101 9 0.531 -0.053 -0.014 0.17 67 0.510 -0.088 0.291 0.380 10 0.588 0.023 -0.101 -0.06 68 0.120 -0.047 -0.259 0.436 11 0.434 0.617 -0.108 -0.01 69 0.494 -0.153 0.071 -0.010 12 0.338 0.576 -0.214 -0.21 70 0.637 -0.323 0.158 0.073 13 0.280 0.276 -0.214 -0.21 71 0.635 -0.246 0.107 0.018 14 0.161 0.076 -0.327 0.39 72 0.626 -0.211 -0.001 0.156 15 0.292 -0.196 0.132 0.16 1.32 0.16 1.32 0.16 < | 63 | 0.310 | 0.171 | 0.057 | 0.100 | 6 | 0.454 | 0.316 | 0.300 | -0.020 |
| 66 0.384 -0.092 0.123 0.101 9 0.531 -0.053 -0.014 0.17 67 0.510 -0.088 0.291 0.380 10 0.588 0.023 -0.101 -0.06 68 0.120 -0.047 -0.259 0.436 11 0.434 0.617 -0.108 -0.00 69 0.494 -0.153 0.071 -0.010 12 0.338 0.570 0.118 -0.11 70 0.637 -0.323 0.158 0.073 13 0.280 0.276 -0.214 -0.21 71 0.635 -0.246 0.107 0.018 14 0.161 0.076 -0.327 0.39 72 0.626 -0.221 -0.001 0.156 15 0.292 -0.196 0.132 0.16 73 0.462 0.039 0.336 0.448 16 0.354 -0.292 0.101 -0.27 74 0.531 -0.266 <t< td=""><td>64</td><td>0.133</td><td>0.658</td><td>1.330</td><td>-0.104</td><td>7</td><td>0.309</td><td>0.289</td><td>-0.035</td><td>0.158</td></t<> | 64 | 0.133 | 0.658 | 1.330 | -0.104 | 7 | 0.309 | 0.289 | -0.035 | 0.158 |
| 67 0.510 -0.088 0.291 0.380 10 0.588 0.023 -0.101 -0.06 68 0.120 -0.047 -0.259 0.436 11 0.434 0.617 -0.108 -0.00 69 0.494 -0.153 0.071 -0.010 12 0.338 0.570 0.118 -0.17 70 0.637 -0.323 0.158 0.073 13 0.280 0.276 -0.214 -0.21 71 0.635 -0.246 0.107 0.018 14 0.161 0.076 -0.327 0.33 72 0.626 -0.211 -0.001 0.156 15 0.292 -0.196 0.132 0.16 73 0.462 0.039 0.336 0.448 16 0.354 -0.292 0.101 -0.25 74 0.531 -0.286 -0.022 -0.013 17 0.020 0.084 -0.097 -0.41 75 0.485 -0.079 | 65 | 0.348 | 0.170 | 0.208 | -0.121 | 8 | 0.692 | 0.003 | 0.488 | 0.549 |
| 68 0.120 -0.047 -0.259 0.436 11 0.434 0.617 -0.108 -0.00 69 0.494 -0.153 0.071 -0.010 12 0.338 0.570 0.118 -0.17 70 0.637 -0.323 0.158 0.073 13 0.280 0.276 -0.214 -0.21 71 0.635 -0.246 0.107 0.018 14 0.161 0.076 -0.327 0.39 72 0.626 -0.211 -0.001 0.156 15 0.292 -0.196 0.132 0.16 73 0.462 0.039 0.336 0.448 16 0.354 -0.292 0.101 -0.22 74 0.531 -0.286 -0.022 -0.113 17 0.020 0.084 -0.097 0.47 75 0.485 -0.079 0.202 0.050 18 0.121 -0.167 0.158 0.17 75 0.445 0.0079 < | 66 | 0.384 | -0.092 | 0.123 | 0.101 | 9 | 0.531 | -0.053 | -0.014 | 0.175 |
| 69 0.494 -0.153 0.071 -0.010 12 0.338 0.570 0.118 -0.11 70 0.637 -0.323 0.158 0.073 13 0.280 0.276 -0.214 -0.21 71 0.635 -0.246 0.107 0.018 14 0.161 0.076 -0.327 0.39 72 0.626 -0.211 -0.001 0.156 15 0.292 -0.196 0.132 0.16 73 0.462 0.039 0.336 0.448 16 0.354 -0.292 0.101 -0.25 74 0.531 -0.286 -0.022 -0.113 17 -0.020 0.084 -0.097 -0.42 75 0.485 -0.079 0.202 0.050 18 0.121 -0.167 0.158 0.19 76 1.022 0.866 -0.188 -0.471 19 0.213 0.017 -0.095 0.14 77 0.410 0.000 < | 67 | 0.510 | -0.088 | 0.291 | 0.380 | 10 | 0.588 | 0.023 | -0.101 | -0.042 |
| 70 0.637 -0.323 0.158 0.073 13 0.280 0.276 -0.214 -0.27 71 0.635 -0.246 0.107 0.018 14 0.161 0.076 -0.327 0.38 72 0.626 -0.211 -0.001 0.156 15 0.292 -0.196 0.132 0.16 73 0.462 0.039 0.336 0.448 16 0.354 -0.292 0.101 -0.25 74 0.531 -0.286 -0.022 -0.050 18 0.121 -0.167 0.158 0.19 75 0.485 -0.079 0.202 0.050 18 0.121 -0.167 0.158 0.19 76 1.022 0.866 -0.188 -0.471 19 0.213 0.017 -0.095 -0.17 77 0.410 0.000 -0.012 -0.117 20 0.085 -0.517 -0.213 0.28 78 0.312 0.054 < | 68 | 0.120 | -0.047 | -0.259 | 0.436 | 11 | 0.434 | 0.617 | -0.108 | -0.002 |
| 71 0.635 -0.246 0.107 0.018 14 0.161 0.076 -0.327 0.33 72 0.626 -0.211 -0.001 0.156 15 0.292 -0.196 0.132 0.16 73 0.462 0.039 0.336 0.448 16 0.354 -0.292 0.101 -0.25 74 0.531 -0.286 -0.022 -0.113 17 0.020 0.084 -0.097 -0.47 75 0.485 -0.079 0.202 0.050 18 0.121 -0.167 0.158 0.14 76 1.022 0.866 -0.188 -0.471 19 0.213 0.017 -0.095 -0.14 77 0.410 0.000 -0.012 -0.117 20 0.085 -0.517 -0.213 0.28 78 0.312 0.054 -0.101 0.017 22 0.483 -0.187 -0.065 -0.17 80 0.486 -0.148 | 69 | 0.494 | -0.153 | 0.071 | -0.010 | 12 | 0.338 | 0.570 | 0.118 | -0.118 |
| 72 0.626 -0.211 -0.001 0.156 15 0.292 -0.196 0.132 0.162 73 0.462 0.039 0.336 0.448 16 0.354 -0.292 0.101 -0.25 74 0.531 -0.286 -0.022 -0.113 17 0.020 0.084 -0.097 -0.47 75 0.485 -0.079 0.202 0.050 18 0.121 -0.167 0.158 0.19 76 1.022 0.866 -0.188 -0.471 19 0.213 0.017 -0.095 -0.14 77 0.410 0.000 -0.012 -0.117 20 0.085 -0.517 -0.213 0.02 78 0.435 0.092 0.328 -0.355 21 0.278 -0.328 0.037 -0.21 80 0.486 -0.148 0.080 0.126 23 0.249 -0.335 -0.069 0.03 81 0.371 -0.075 | 70 | 0.637 | -0.323 | 0.158 | 0.073 | 13 | 0.280 | 0.276 | -0.214 | -0.211 |
| 73 0.462 0.039 0.336 0.448 16 0.354 -0.292 0.101 -0.25 74 0.531 -0.286 -0.022 -0.113 17 0.020 0.084 -0.097 -0.47 75 0.485 -0.079 0.202 0.050 18 0.121 -0.167 0.158 0.19 76 1.022 0.866 -0.188 -0.471 19 0.213 0.017 -0.095 -0.14 77 0.410 0.000 -0.012 -0.117 20 0.085 -0.517 -0.213 0.22 78 0.435 0.092 0.328 -0.355 21 0.278 -0.328 0.037 -0.22 79 0.312 0.054 -0.101 0.017 22 0.483 -0.187 -0.065 -0.17 80 0.486 -0.148 0.080 0.126 23 0.249 -0.335 -0.065 0.014 24 0.524 -0.246 0.097 | 71 | 0.635 | -0.246 | 0.107 | 0.018 | 14 | 0.161 | 0.076 | -0.327 | 0.390 |
| 74 0.531 -0.286 -0.022 -0.113 17 0.020 0.084 -0.097 -0.47 75 0.485 -0.079 0.202 0.050 18 0.121 -0.167 0.158 0.19 76 1.022 0.866 -0.188 -0.471 19 0.213 0.017 -0.095 -0.14 77 0.410 0.000 -0.012 -0.117 20 0.085 -0.517 -0.213 0.28 78 0.435 0.092 0.328 -0.355 21 0.278 -0.328 0.037 -0.26 80 0.486 -0.148 0.080 0.126 23 0.249 -0.335 -0.065 -0.17 80 0.486 -0.148 0.080 0.126 23 0.249 -0.335 -0.069 0.03 81 0.371 -0.075 -0.005 0.014 24 0.524 -0.246 0.097 -0.13 82 0.366 -0.097 | 72 | 0.626 | -0.211 | -0.001 | 0.156 | 15 | 0.292 | -0.196 | 0.132 | 0.164 |
| 75 0.485 -0.079 0.202 0.050 18 0.121 -0.167 0.158 0.18 76 1.022 0.866 -0.188 -0.471 19 0.213 0.017 -0.095 -0.14 77 0.410 0.000 -0.012 -0.117 20 0.085 -0.517 -0.213 0.28 78 0.435 0.092 0.328 -0.355 21 0.278 -0.328 0.037 -0.26 79 0.312 0.054 -0.101 0.017 22 0.483 -0.187 -0.065 -0.17 80 0.486 -0.148 0.080 0.126 23 0.249 -0.335 -0.069 0.03 81 0.371 -0.075 -0.005 0.014 24 0.524 -0.246 0.097 -0.13 82 0.366 -0.097 0.140 0.162 25 0.316 0.415 0.097 0.05 83 0.389 -0.050 | 73 | 0.462 | 0.039 | 0.336 | 0.448 | 16 | 0.354 | -0.292 | 0.101 | -0.292 |
| 76 1.022 0.866 -0.188 -0.471 19 0.213 0.017 -0.095 -0.14 77 0.410 0.000 -0.012 -0.117 20 0.085 -0.517 -0.213 0.28 78 0.435 0.092 0.328 -0.355 21 0.278 -0.328 0.037 -0.26 79 0.312 0.054 -0.101 0.017 22 0.483 -0.187 -0.065 -0.17 80 0.486 -0.148 0.080 0.126 23 0.249 -0.335 -0.069 0.03 81 0.371 -0.075 -0.005 0.014 24 0.524 -0.246 0.097 -0.13 82 0.366 -0.097 0.140 0.162 25 0.316 0.415 0.097 0.05 83 0.389 -0.050 0.008 0.154 26 0.532 0.299 0.298 0.33 84 0.320 -0.099 | 74 | 0.531 | -0.286 | -0.022 | -0.113 | 17 | 0.020 | 0.084 | -0.097 | -0.474 |
| 77 0.410 0.000 -0.012 -0.117 20 0.085 -0.517 -0.213 0.28 78 0.435 0.092 0.328 -0.355 21 0.278 -0.328 0.037 -0.20 79 0.312 0.054 -0.101 0.017 22 0.483 -0.187 -0.065 -0.17 80 0.486 -0.148 0.080 0.126 23 0.249 -0.335 -0.069 0.03 81 0.371 -0.075 -0.005 0.014 24 0.524 -0.246 0.097 -0.13 82 0.366 -0.097 0.140 0.162 25 0.316 0.415 0.097 0.05 83 0.389 -0.050 0.008 0.154 26 0.532 0.299 0.298 0.33 84 0.320 -0.099 0.047 0.057 27 0.307 0.706 0.463 0.14 85 0.438 -0.139 <td< td=""><td>75</td><td>0.485</td><td>-0.079</td><td>0.202</td><td>0.050</td><td>18</td><td>0.121</td><td>-0.167</td><td>0.158</td><td>0.197</td></td<> | 75 | 0.485 | -0.079 | 0.202 | 0.050 | 18 | 0.121 | -0.167 | 0.158 | 0.197 |
| 78 0.435 0.092 0.328 -0.355 21 0.278 -0.328 0.037 -0.20 79 0.312 0.054 -0.101 0.017 22 0.483 -0.187 -0.065 -0.17 80 0.486 -0.148 0.080 0.126 23 0.249 -0.335 -0.069 0.03 81 0.371 -0.075 -0.005 0.014 24 0.524 -0.246 0.097 -0.13 82 0.366 -0.097 0.140 0.162 25 0.316 0.415 0.097 0.05 83 0.389 -0.050 0.008 0.154 26 0.532 0.299 0.298 0.33 84 0.320 -0.099 0.047 0.057 27 0.307 0.706 0.463 0.14 85 0.438 -0.139 0.129 0.084 28 0.330 -0.017 0.290 0.12 86 0.516 -0.120 0 | 76 | 1.022 | 0.866 | -0.188 | -0.471 | 19 | 0.213 | 0.017 | -0.095 | -0.147 |
| 79 0.312 0.054 -0.101 0.017 22 0.483 -0.187 -0.065 -0.17 80 0.486 -0.148 0.080 0.126 23 0.249 -0.335 -0.069 0.03 81 0.371 -0.075 -0.005 0.014 24 0.524 -0.246 0.097 -0.13 82 0.366 -0.097 0.140 0.162 25 0.316 0.415 0.097 0.05 83 0.389 -0.050 0.008 0.154 26 0.532 0.299 0.298 0.33 84 0.320 -0.099 0.047 0.057 27 0.307 0.706 0.463 0.14 85 0.438 -0.139 0.129 0.084 28 0.330 -0.017 0.290 0.12 86 0.516 -0.120 0.098 0.108 29 0.400 -0.154 0.120 -0.07 87 0.449 0.098 0. | 77 | 0.410 | 0.000 | -0.012 | -0.117 | 20 | 0.085 | -0.517 | -0.213 | 0.289 |
| 80 0.486 -0.148 0.080 0.126 23 0.249 -0.335 -0.069 0.03 81 0.371 -0.075 -0.005 0.014 24 0.524 -0.246 0.097 -0.13 82 0.366 -0.097 0.140 0.162 25 0.316 0.415 0.097 0.05 83 0.389 -0.050 0.008 0.154 26 0.532 0.299 0.298 0.33 84 0.320 -0.099 0.047 0.057 27 0.307 0.706 0.463 0.14 85 0.438 -0.139 0.129 0.084 28 0.330 -0.017 0.290 0.12 86 0.516 -0.120 0.098 0.108 29 0.400 -0.154 0.120 -0.07 87 0.449 0.098 0.028 0.108 30 0.610 -0.004 0.215 -0.02 88 0.502 -0.230 -0. | 78 | 0.435 | 0.092 | 0.328 | -0.355 | 21 | 0.278 | -0.328 | 0.037 | -0.206 |
| 81 0.371 -0.075 -0.005 0.014 24 0.524 -0.246 0.097 -0.13 82 0.366 -0.097 0.140 0.162 25 0.316 0.415 0.097 0.05 83 0.389 -0.050 0.008 0.154 26 0.532 0.299 0.298 0.33 84 0.320 -0.099 0.047 0.057 27 0.307 0.706 0.463 0.14 85 0.438 -0.139 0.129 0.084 28 0.330 -0.017 0.290 0.12 86 0.516 -0.120 0.098 0.108 29 0.400 -0.154 0.120 -0.07 87 0.449 0.098 0.028 0.108 30 0.610 -0.004 0.215 -0.02 88 0.502 -0.230 -0.093 0.076 31 0.475 0.831 -0.284 -0.00 89 0.427 -0.172 0. | 79 | 0.312 | 0.054 | -0.101 | 0.017 | 22 | 0.483 | -0.187 | -0.065 | -0.178 |
| 82 0.366 -0.097 0.140 0.162 25 0.316 0.415 0.097 0.058 83 0.389 -0.050 0.008 0.154 26 0.532 0.299 0.298 0.33 84 0.320 -0.099 0.047 0.057 27 0.307 0.706 0.463 0.14 85 0.438 -0.139 0.129 0.084 28 0.330 -0.017 0.290 0.12 86 0.516 -0.120 0.098 0.108 29 0.400 -0.154 0.120 -0.07 87 0.449 0.098 0.028 0.108 30 0.610 -0.004 0.215 -0.02 88 0.502 -0.230 -0.093 0.076 31 0.475 0.831 -0.284 -0.00 89 0.427 -0.172 0.063 0.014 32 0.179 0.289 -0.384 0.21 90 0.689 0.052 -0.3 | 80 | 0.486 | -0.148 | 0.080 | 0.126 | 23 | 0.249 | -0.335 | -0.069 | 0.039 |
| 83 0.389 -0.050 0.008 0.154 26 0.532 0.299 0.298 0.33 84 0.320 -0.099 0.047 0.057 27 0.307 0.706 0.463 0.14 85 0.438 -0.139 0.129 0.084 28 0.330 -0.017 0.290 0.12 86 0.516 -0.120 0.098 0.108 29 0.400 -0.154 0.120 -0.07 87 0.449 0.098 0.028 0.108 30 0.610 -0.004 0.215 -0.02 88 0.502 -0.230 -0.093 0.076 31 0.475 0.831 -0.284 -0.00 89 0.427 -0.172 0.063 0.014 32 0.179 0.289 -0.384 0.21 90 0.689 0.052 -0.326 -0.016 33 -0.025 0.488 -0.075 -0.22 91 0.395 0.072 0 | 81 | 0.371 | -0.075 | -0.005 | 0.014 | 24 | 0.524 | -0.246 | 0.097 | -0.135 |
| 84 0.320 -0.099 0.047 0.057 27 0.307 0.706 0.463 0.14 85 0.438 -0.139 0.129 0.084 28 0.330 -0.017 0.290 0.12 86 0.516 -0.120 0.098 0.108 29 0.400 -0.154 0.120 -0.07 87 0.449 0.098 0.028 0.108 30 0.610 -0.004 0.215 -0.02 88 0.502 -0.230 -0.093 0.076 31 0.475 0.831 -0.284 -0.00 89 0.427 -0.172 0.063 0.014 32 0.179 0.289 -0.384 0.21 90 0.689 0.052 -0.326 -0.016 33 -0.025 0.488 -0.075 -0.22 91 0.395 0.072 0.033 -0.005 34 0.260 -0.294 0.004 -0.05 92 0.365 -0.146 <t< td=""><td></td><td>0.366</td><td>-0.097</td><td>0.140</td><td>0.162</td><td>25</td><td>0.316</td><td>0.415</td><td>0.097</td><td>0.055</td></t<> | | 0.366 | -0.097 | 0.140 | 0.162 | 25 | 0.316 | 0.415 | 0.097 | 0.055 |
| 85 0.438 -0.139 0.129 0.084 28 0.330 -0.017 0.290 0.12 86 0.516 -0.120 0.098 0.108 29 0.400 -0.154 0.120 -0.07 87 0.449 0.098 0.028 0.108 30 0.610 -0.004 0.215 -0.02 88 0.502 -0.230 -0.093 0.076 31 0.475 0.831 -0.284 -0.00 89 0.427 -0.172 0.063 0.014 32 0.179 0.289 -0.384 0.21 90 0.689 0.052 -0.326 -0.016 33 -0.025 0.488 -0.075 -0.22 91 0.395 0.072 0.033 -0.005 34 0.260 -0.294 0.004 -0.05 92 0.365 -0.146 0.053 0.027 35 -0.058 -0.122 0.279 0.30 93 0.437 -0.202 | 83 | 0.389 | -0.050 | 0.008 | 0.154 | 26 | 0.532 | 0.299 | 0.298 | 0.338 |
| 86 0.516 -0.120 0.098 0.108 29 0.400 -0.154 0.120 -0.07 87 0.449 0.098 0.028 0.108 30 0.610 -0.004 0.215 -0.02 88 0.502 -0.230 -0.093 0.076 31 0.475 0.831 -0.284 -0.00 89 0.427 -0.172 0.063 0.014 32 0.179 0.289 -0.384 0.21 90 0.689 0.052 -0.326 -0.016 33 -0.025 0.488 -0.075 -0.22 91 0.395 0.072 0.033 -0.005 34 0.260 -0.294 0.004 -0.05 92 0.365 -0.146 0.053 0.027 35 -0.058 -0.122 0.279 0.30 93 0.437 -0.202 -0.002 0.145 36 0.214 0.207 -0.228 0.07 94 0.500 -0.116 | | | -0.099 | 0.047 | | 27 | 0.307 | 0.706 | 0.463 | 0.149 |
| 87 0.449 0.098 0.028 0.108 30 0.610 -0.004 0.215 -0.02 88 0.502 -0.230 -0.093 0.076 31 0.475 0.831 -0.284 -0.00 89 0.427 -0.172 0.063 0.014 32 0.179 0.289 -0.384 0.21 90 0.689 0.052 -0.326 -0.016 33 -0.025 0.488 -0.075 -0.22 91 0.395 0.072 0.033 -0.005 34 0.260 -0.294 0.004 -0.05 92 0.365 -0.146 0.053 0.027 35 -0.058 -0.122 0.279 0.30 93 0.437 -0.202 -0.002 0.145 36 0.214 0.207 -0.228 0.07 94 0.500 -0.116 0.077 -0.249 37 -0.084 -0.079 -0.030 0.11 95 0.380 0.389 | 85 | | -0.139 | | | 28 | 0.330 | -0.017 | 0.290 | 0.127 |
| 88 0.502 -0.230 -0.093 0.076 31 0.475 0.831 -0.284 -0.00 89 0.427 -0.172 0.063 0.014 32 0.179 0.289 -0.384 0.21 90 0.689 0.052 -0.326 -0.016 33 -0.025 0.488 -0.075 -0.22 91 0.395 0.072 0.033 -0.005 34 0.260 -0.294 0.004 -0.05 92 0.365 -0.146 0.053 0.027 35 -0.058 -0.122 0.279 0.30 93 0.437 -0.202 -0.002 0.145 36 0.214 0.207 -0.228 0.07 94 0.500 -0.116 0.077 -0.249 37 -0.084 -0.079 -0.030 0.11 95 0.380 0.389 -0.021 0.059 38 0.480 0.365 -0.036 -0.07 96 0.575 0.223 | | 0.516 | -0.120 | 0.098 | 0.108 | 29 | 0.400 | -0.154 | 0.120 | -0.070 |
| 89 0.427 -0.172 0.063 0.014 32 0.179 0.289 -0.384 0.21 90 0.689 0.052 -0.326 -0.016 33 -0.025 0.488 -0.075 -0.22 91 0.395 0.072 0.033 -0.005 34 0.260 -0.294 0.004 -0.05 92 0.365 -0.146 0.053 0.027 35 -0.058 -0.122 0.279 0.30 93 0.437 -0.202 -0.002 0.145 36 0.214 0.207 -0.228 0.07 94 0.500 -0.116 0.077 -0.249 37 -0.084 -0.079 -0.030 0.11 95 0.380 0.389 -0.021 0.059 38 0.480 0.365 -0.036 -0.07 96 0.575 0.223 0.016 0.210 39 0.361 0.625 0.069 0.11 97 0.204 0.454 < | | | | | | 30 | 0.610 | -0.004 | 0.215 | -0.021 |
| 90 0.689 0.052 -0.326 -0.016 33 -0.025 0.488 -0.075 -0.22 91 0.395 0.072 0.033 -0.005 34 0.260 -0.294 0.004 -0.05 92 0.365 -0.146 0.053 0.027 35 -0.058 -0.122 0.279 0.30 93 0.437 -0.202 -0.002 0.145 36 0.214 0.207 -0.228 0.07 94 0.500 -0.116 0.077 -0.249 37 -0.084 -0.079 -0.030 0.11 95 0.380 0.389 -0.021 0.059 38 0.480 0.365 -0.036 -0.07 96 0.575 0.223 0.016 0.210 39 0.361 0.625 0.069 0.11 97 0.204 0.454 -0.076 0.023 40 0.303 -0.095 0.019 0.26 98 0.329 -0.212 | | | | | | 31 | 0.475 | 0.831 | -0.284 | -0.004 |
| 91 0.395 0.072 0.033 -0.005 34 0.260 -0.294 0.004 -0.05 92 0.365 -0.146 0.053 0.027 35 -0.058 -0.122 0.279 0.30 93 0.437 -0.202 -0.002 0.145 36 0.214 0.207 -0.228 0.07 94 0.500 -0.116 0.077 -0.249 37 -0.084 -0.079 -0.030 0.11 95 0.380 0.389 -0.021 0.059 38 0.480 0.365 -0.036 -0.07 96 0.575 0.223 0.016 0.210 39 0.361 0.625 0.069 0.11 97 0.204 0.454 -0.076 0.023 40 0.303 -0.095 0.019 0.26 98 0.329 -0.212 0.175 0.143 41 0.330 0.476 0.046 -0.17 | | | | | | 32 | 0.179 | 0.289 | -0.384 | 0.212 |
| 92 0.365 -0.146 0.053 0.027 35 -0.058 -0.122 0.279 0.30 93 0.437 -0.202 -0.002 0.145 36 0.214 0.207 -0.228 0.07 94 0.500 -0.116 0.077 -0.249 37 -0.084 -0.079 -0.030 0.11 95 0.380 0.389 -0.021 0.059 38 0.480 0.365 -0.036 -0.07 96 0.575 0.223 0.016 0.210 39 0.361 0.625 0.069 0.11 97 0.204 0.454 -0.076 0.023 40 0.303 -0.095 0.019 0.26 98 0.329 -0.212 0.175 0.143 41 0.330 0.476 0.046 -0.17 | | | | | | 33 | -0.025 | 0.488 | -0.075 | -0.222 |
| 93 0.437 -0.202 -0.002 0.145 36 0.214 0.207 -0.228 0.07 94 0.500 -0.116 0.077 -0.249 37 -0.084 -0.079 -0.030 0.11 95 0.380 0.389 -0.021 0.059 38 0.480 0.365 -0.036 -0.07 96 0.575 0.223 0.016 0.210 39 0.361 0.625 0.069 0.11 97 0.204 0.454 -0.076 0.023 40 0.303 -0.095 0.019 0.26 98 0.329 -0.212 0.175 0.143 41 0.330 0.476 0.046 -0.17 | | | | | | 34 | 0.260 | -0.294 | 0.004 | -0.053 |
| 94 0.500 -0.116 0.077 -0.249 37 -0.084 -0.079 -0.030 0.11 95 0.380 0.389 -0.021 0.059 38 0.480 0.365 -0.036 -0.07 96 0.575 0.223 0.016 0.210 39 0.361 0.625 0.069 0.11 97 0.204 0.454 -0.076 0.023 40 0.303 -0.095 0.019 0.26 98 0.329 -0.212 0.175 0.143 41 0.330 0.476 0.046 -0.17 | | | | | | 35 | -0.058 | -0.122 | 0.279 | 0.303 |
| 95 0.380 0.389 -0.021 0.059 38 0.480 0.365 -0.036 -0.07 96 0.575 0.223 0.016 0.210 39 0.361 0.625 0.069 0.11 97 0.204 0.454 -0.076 0.023 40 0.303 -0.095 0.019 0.26 98 0.329 -0.212 0.175 0.143 41 0.330 0.476 0.046 -0.17 | | | | | | 36 | 0.214 | 0.207 | -0.228 | 0.078 |
| 96 0.575 0.223 0.016 0.210 39 0.361 0.625 0.069 0.11 97 0.204 0.454 -0.076 0.023 40 0.303 -0.095 0.019 0.26 98 0.329 -0.212 0.175 0.143 41 0.330 0.476 0.046 -0.17 | | | | | | 37 | -0.084 | -0.079 | -0.030 | 0.116 |
| 97 0.204 0.454 -0.076 0.023 40 0.303 -0.095 0.019 0.26 98 0.329 -0.212 0.175 0.143 41 0.330 0.476 0.046 -0.17 | | | | | | 38 | 0.480 | 0.365 | -0.036 | -0.074 |
| 98 0.329 -0.212 0.175 0.143 41 0.330 0.476 0.046 -0.17 | | | | | | 39 | 0.361 | 0.625 | 0.069 | 0.110 |
| 11 0.000 0.110 0.010 | | | | | | 40 | | -0.095 | 0.019 | 0.268 |
| | | | | | | 41 | 0.330 | | 0.046 | -0.178 |
| | | | | | | | 0.497 | 0.212 | -0.014 | 0.104 |
| <u>100 0.580 -0.105 0.110 0.198</u> 43 0.252 -0.057 -0.191 0.31 | 100 | 0.580 | -0.105 | 0.110 | 0.198 | 43 | 0.252 | -0.057 | -0.191 | 0.317 |

| 44 | 0.083 | -0.349 | 0.126 | -0.129 | 92 | 0.531 | -0.172 | -0.234 | 0.012 |
|----|--------|--------|--------|--------|-----|-------|--------|--------|--------|
| 45 | 0.274 | 0.249 | 0.172 | -0.045 | 93 | 0.567 | 0.033 | -0.275 | -0.029 |
| 46 | 0.309 | 0.521 | -0.232 | -0.083 | 94 | 0.475 | 0.017 | 0.233 | 0.250 |
| 47 | 0.341 | 0.492 | -0.314 | 0.157 | 95 | 0.242 | 0.272 | 0.148 | 0.267 |
| 48 | 0.278 | 0.146 | 0.052 | 0.128 | 96 | 0.546 | -0.089 | -0.022 | 0.170 |
| 49 | 0.436 | 0.773 | -0.004 | -0.027 | 97 | 0.214 | 0.101 | -0.029 | -0.042 |
| 50 | -0.186 | 0.228 | 0.611 | -0.212 | 98 | 0.294 | 0.061 | -0.235 | -0.008 |
| 51 | 0.588 | -0.026 | -0.229 | -0.449 | 99 | 0.334 | -0.303 | 0.059 | 0.241 |
| 52 | 0.625 | -0.505 | 0.101 | -0.254 | 100 | 0.305 | 0.287 | 0.199 | 0.156 |
| 53 | 0.693 | -0.431 | -0.072 | -0.134 | | | | | |

Table B.6. Factor Loadings for GCVR- High

| | 0.500 | 5.101 | 5.51 <u>L</u> | 301 | | | | | | | | |
|----|--------|--------|---------------|--------|-------------|------------|----------|--|--|--|--|--|
| 54 | 0.439 | 0.246 | -0.642 | -0.113 | Table B | .6. Factor | Loadings | | | | | |
| 55 | 0.540 | -0.072 | -0.318 | -0.174 | Proficiency | | | | | | | |
| 56 | 0.500 | -0.304 | 0.322 | -0.355 | Item | | Factor I | | | | | |
| 57 | 0.560 | 0.199 | 0.412 | -0.285 | 1.0111 | 1 | 2 | | | | | |
| 58 | 0.357 | -0.514 | 0.397 | -0.155 | 1 | 0.355 | 0.024 | | | | | |
|) | 0.454 | -0.124 | 0.075 | -0.455 | 2 | 0.303 | 0.184 | | | | | |
| 0 | 0.543 | 0.078 | -0.240 | -0.537 | 3 | 0.404 | 0.128 | | | | | |
| | 0.559 | 0.301 | -0.147 | 0.113 | 4 | 0.390 | -0.307 | | | | | |
| | 0.197 | 0.163 | -0.082 | -0.044 | 5 | 0.153 | 0.179 | | | | | |
| | 0.315 | 0.270 | 0.036 | -0.043 | 6 | 0.565 | -0.224 | | | | | |
| | 0.428 | -0.584 | -0.188 | 0.038 | 7 | 0.179 | 0.271 | | | | | |
| | 0.529 | -0.092 | 0.235 | -0.098 | 8 | 0.566 | -0.145 | | | | | |
| i | 0.451 | -0.472 | 0.050 | -0.199 | 9 | 0.160 | 0.298 | | | | | |
| | 0.343 | -0.135 | 0.131 | -0.081 | 10 | 0.309 | 0.368 | | | | | |
| 3 | 0.425 | -0.159 | 0.074 | -0.095 | 11 | 0.323 | -0.263 | | | | | |
|) | 0.204 | -0.319 | 0.444 | 0.113 | 12 | 0.534 | -0.013 | | | | | |
| | 0.631 | -0.095 | 0.061 | 0.106 | 13 | 0.416 | -0.227 | | | | | |
| | 0.451 | -0.396 | -0.096 | -0.244 | 14 | 0.359 | 0.526 | | | | | |
| | -0.175 | -0.028 | 0.187 | -0.019 | 15 | 0.304 | 0.141 | | | | | |
| | 0.271 | -0.150 | 0.244 | 0.302 | 16 | 0.417 | 0.255 | | | | | |
| | 0.357 | -0.116 | -0.160 | 0.336 | 17 | 0.143 | 0.235 | | | | | |
| | 0.689 | -0.203 | 0.018 | 0.174 | 18 | 0.216 | -0.265 | | | | | |
| | 0.365 | -0.301 | -0.283 | 0.056 | 19 | 0.118 | 0.725 | | | | | |
| | 0.352 | -0.048 | -0.295 | -0.092 | 20 | 0.101 | 0.134 | | | | | |
| | 0.436 | -0.292 | 0.097 | -0.211 | 21 | 0.294 | 0.134 | | | | | |
| | 0.120 | -0.284 | 0.274 | -0.134 | 22 | 0.277 | 0.270 | | | | | |
| | 0.433 | -0.159 | 0.389 | -0.221 | 23 | 0.693 | 0.275 | | | | | |
| | 0.193 | -0.289 | -0.050 | -0.040 | 24 | 0.489 | 0.209 | | | | | |
| | 0.295 | 0.139 | 0.313 | 0.160 | 25 | 0.385 | -0.125 | | | | | |
| | 0.214 | -0.590 | -0.325 | 0.413 | 26 | 0.391 | -0.482 | | | | | |
| 1 | 0.474 | -0.221 | -0.355 | 0.031 | 27 | 0.493 | 0.192 | | | | | |
| 5 | 0.233 | -0.108 | 0.274 | 0.280 | 28 | 0.494 | -0.022 | | | | | |
| 6 | 0.554 | -0.202 | -0.147 | 0.101 | 29 | 0.391 | 0.250 | | | | | |
| • | 0.338 | -0.148 | -0.044 | 0.114 | 30 | 0.393 | 0.371 | | | | | |
| 8 | 0.519 | 0.109 | 0.099 | 0.219 | 31 | 0.307 | 0.372 | | | | | |
| 9 | 0.545 | -0.261 | -0.113 | -0.044 | 32 | 0.182 | 0.115 | | | | | |
| 0 | 0.241 | -0.434 | -0.272 | 0.333 | 33 | 0.248 | 0.199 | | | | | |
| 1 | 0.426 | -0.043 | -0.434 | 0.217 | | | | | | | | |
| | | | | | | | | | | | | |

| 34 | 0.457 | 0.090 | 0.153 | -0.092 | 82 | 0.157 | 0.344 | -0.292 | 0.172 |
|----|--------|--------|--------|--------|-----|--------|--------|--------|--------|
| 35 | 0.107 | 0.456 | -0.033 | -0.154 | 83 | 0.108 | 0.386 | 0.180 | -0.157 |
| 36 | 0.176 | 0.213 | -0.102 | 0.158 | 84 | 0.068 | 0.400 | 0.094 | 0.033 |
| 37 | -0.025 | 0.257 | -0.114 | 0.007 | 85 | 0.215 | 0.339 | 0.092 | 0.015 |
| 38 | 0.390 | 0.282 | -0.115 | 0.069 | 86 | 0.355 | -0.200 | 0.209 | 0.093 |
| 39 | 0.134 | 0.371 | -0.090 | 0.205 | 87 | 0.213 | 0.204 | 0.276 | 0.078 |
| 40 | 0.336 | -0.101 | 0.071 | -0.074 | 88 | 0.283 | 0.417 | 0.080 | 0.071 |
| 41 | 0.380 | 0.181 | -0.022 | 0.088 | 89 | 0.144 | 0.265 | 0.327 | 0.545 |
| 42 | 0.369 | 0.053 | 0.051 | 0.037 | 90 | 0.304 | 0.431 | 0.347 | -0.172 |
| 43 | 0.172 | 0.148 | 0.093 | -0.060 | 91 | 0.064 | 0.427 | 0.098 | -0.042 |
| 44 | 0.310 | 0.167 | 0.053 | -0.026 | 92 | 0.288 | 0.282 | 0.032 | -0.048 |
| 45 | 0.167 | 0.246 | -0.394 | 0.123 | 93 | 0.229 | 0.142 | 0.184 | 0.044 |
| 46 | 0.172 | -0.201 | -0.079 | 0.070 | 94 | 0.130 | 0.495 | 0.055 | 0.074 |
| 47 | 0.336 | 0.271 | -0.308 | 0.220 | 95 | 0.109 | 0.285 | -0.038 | 0.164 |
| 48 | 0.226 | 0.376 | -0.018 | -0.044 | 96 | 0.181 | 0.307 | 0.110 | 0.030 |
| 49 | 0.686 | -0.219 | -0.280 | 0.210 | 97 | -0.036 | 0.299 | -0.049 | 0.154 |
| 50 | 0.167 | 0.187 | -0.061 | -0.081 | 98 | 0.204 | 0.083 | 0.113 | 0.158 |
| 51 | 0.293 | -0.159 | -0.215 | 0.750 | 99 | 0.206 | 0.354 | 0.131 | 0.021 |
| 52 | 0.086 | -0.534 | 0.341 | 0.614 | 100 | 0.411 | 0.109 | 0.122 | 0.002 |
| 53 | 0.320 | -0.011 | -0.176 | 0.533 | | | | | |
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0.532

0.272

0.348

0.475

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0.095

0.377

0.205

0.429

0.389

0.507

0.375

0.473

0.568

0.565

0.503

0.477

-0.122

0.453

0.576

0.326

0.453

0.187

0.060

-0.525

Table B.7. Factor Loadings for GCVR-Low Proficiency

| | | | I dole L | I acto | Louding | 0 101 00 1 | L |
|-------|--------|--------|----------|----------|----------|------------|-------|
| .311 | 0.007 | 0.118 | Proficie | ency | _ | | |
| .073 | 0.154 | 0.012 | Item | <u> </u> | Factor L | oadings | |
| 0.562 | -0.454 | -0.374 | | 1 | 2 | 3 | 4 |
| 0.469 | 0.297 | -0.195 | 1 | 0.407 | -0.192 | 0.202 | 0.25 |
| 0.316 | 0.150 | -0.190 | 2 | 0.266 | 0.257 | -0.105 | 0.12 |
|).171 | 0.023 | 0.180 | 3 | 0.234 | 0.053 | 0.055 | 0.03 |
| .424 | 0.135 | 0.160 | 4 | 0.405 | -0.005 | 0.009 | 0.31 |
| .165 | -0.082 | -0.177 | 5 | 0.184 | -0.158 | 0.119 | -0.04 |
| .221 | -0.293 | 0.014 | 6 | 0.305 | -0.023 | -0.164 | 0.20 |
|).211 | 0.595 | 0.296 | 7 | -0.081 | 0.194 | 0.195 | 0.01 |
| .127 | -0.438 | 0.048 | 8 | 0.324 | -0.122 | 0.298 | 0.33 |
| .006 | 0.083 | 0.064 | 9 | 0.013 | 0.329 | -0.060 | 0.19 |
| .239 | 0.411 | 0.445 | 10 | 0.078 | 0.523 | -0.201 | -0.04 |
| 244 | 0.107 | -0.026 | 11 | 0.518 | -0.018 | 0.007 | 0.35 |
| 108 | 0.407 | 0.031 | 12 | 0.087 | -0.080 | 0.030 | 0.39 |
| .432 | 0.215 | 0.193 | 13 | 0.456 | -0.124 | -0.042 | -0.03 |
| .109 | 0.250 | 0.037 | 14 | -0.157 | 0.291 | -0.190 | -0.0 |
| .304 | 0.188 | -0.053 | 15 | 0.464 | 0.147 | 0.108 | 0.04 |
| .402 | 0.170 | -0.036 | 16 | 0.129 | 0.262 | -0.442 | -0.0 |
| .110 | 0.011 | -0.093 | 17 | -0.157 | 0.020 | 0.453 | 0.21 |
| .564 | -0.176 | 0.122 | 18 | 0.264 | -0.217 | 0.342 | 0.00 |
| .144 | 1.653 | -0.254 | 19 | -0.327 | 0.324 | -0.017 | 0.09 |
| .141 | -0.319 | 0.110 | 20 | -0.026 | 0.202 | 0.139 | -0.14 |
| .615 | 0.291 | -0.027 | 21 | 0.157 | -0.065 | 0.223 | 0.06 |
| 096 | 0.019 | -0.180 | 22 | 0.205 | 0.299 | 0.036 | 0.19 |
| .141 | 0.224 | 0.152 | 23 | -0.104 | 0.349 | -0.287 | -0.09 |
| 298 | 0.052 | -0.209 | | | | | |
| | | | | | | | |

| 24 | 0.018 | 0.356 | -0.162 | 0.047 | 72 |
|----|--------|--------|--------|--------|-----|
| 25 | 0.366 | -0.076 | -0.173 | 0.199 | 73 |
| 26 | 0.441 | 0.114 | -0.238 | 0.271 | 74 |
| 27 | -0.019 | 0.083 | -0.073 | 0.433 | 75 |
| 28 | 0.234 | 0.232 | 0.024 | 0.376 | 76 |
| 29 | 0.120 | 0.032 | -0.018 | 0.105 | 77 |
| 30 | -0.049 | 0.689 | -0.133 | 0.014 | 78 |
| 31 | -0.187 | 0.141 | -0.236 | 0.405 | 79 |
| 32 | 0.377 | 0.134 | -0.119 | -0.023 | 80 |
| 33 | 0.116 | -0.195 | 0.091 | 0.132 | 81 |
| 34 | 0.105 | 0.155 | 0.121 | 0.160 | 82 |
| 35 | -0.232 | -0.147 | 0.089 | 0.024 | 83 |
| 36 | 0.081 | 0.251 | 0.124 | 0.169 | 84 |
| 37 | -0.190 | -0.166 | 0.076 | -0.021 | 85 |
| 38 | -0.079 | 0.050 | -0.178 | 0.031 | 86 |
| 39 | -0.112 | 0.264 | -0.080 | 0.174 | 87 |
| 40 | 0.467 | -0.136 | 0.170 | -0.013 | 88 |
| 41 | 0.074 | 0.128 | -0.129 | -0.011 | 89 |
| 42 | 0.284 | 0.005 | -0.115 | 0.166 | 90 |
| 43 | -0.003 | -0.029 | 0.183 | 0.099 | 91 |
| 44 | 0.022 | 0.171 | 0.190 | -0.048 | 92 |
| 45 | 0.039 | 0.118 | 0.118 | 0.009 | 93 |
| 46 | 0.228 | -0.171 | -0.069 | 0.134 | 94 |
| 47 | -0.007 | 0.358 | 0.033 | 0.221 | 95 |
| 48 | -0.154 | 0.177 | 0.242 | -0.049 | 96 |
| 49 | 0.279 | 0.042 | 0.003 | 0.381 | 97 |
| 50 | -0.022 | 0.161 | 0.134 | 0.329 | 98 |
| 51 | 0.687 | 0.158 | -0.134 | -0.119 | 99 |
| 52 | 0.638 | 0.084 | -0.164 | -0.287 | 100 |
| 53 | 0.444 | 0.156 | -0.101 | -0.257 | |
| 54 | 0.524 | 0.070 | -0.097 | -0.003 | |
| 55 | 0.229 | 0.433 | -0.267 | -0.010 | |
| 56 | 0.317 | 0.002 | -0.193 | -0.159 | |
| 57 | 0.764 | -0.358 | -0.012 | -0.065 | |
| 58 | 0.605 | -0.004 | 0.113 | -0.077 | |
| 59 | 0.659 | -0.020 | -0.028 | -0.006 | |
| 60 | 0.495 | 0.036 | -0.101 | -0.103 | |
| 61 | 0.678 | -0.080 | -0.097 | 0.068 | |
| 62 | -0.039 | 0.207 | -0.059 | 0.032 | |
| 63 | 0.132 | -0.020 | -0.096 | 0.036 | |
| 64 | 0.673 | 0.166 | -0.094 | -0.127 | |
| 65 | 0.518 | 0.115 | 0.081 | 0.062 | |
| 66 | 0.176 | 0.360 | 0.092 | -0.179 | |
| 67 | 0.578 | 0.107 | -0.004 | -0.092 | |
| 68 | 0.719 | -0.205 | 0.012 | 0.079 | |
| 69 | -0.030 | 0.025 | 0.139 | -0.140 | |

0.244

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-0.012

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-0.066 -0.045

-0.100 0.134

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71

0.644

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-0.170

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